

Equivalent Loading Frequencies to Simulate Asphalt Layer Pavement Responses Under Dynamic Traffic Loading

Elie Y. Hajj, Ph.D.
Alvaro Ulloa, Ph.D. Candidate
Peter E. Sebaaly, Ph.D.
Raj V. Siddharthan, Ph.D.

University of Nevada Reno

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Introduction



- *Dynamic response* of AC pavements under moving load is a key component for accurate prediction of *flexible pavement performance*.
- *Reliable determination* of pavement responses to *moving load* is essential for a successful mechanistic design procedure.
- *Time and temperature dependency* of asphalt must be considered in the mechanistic analysis response model.

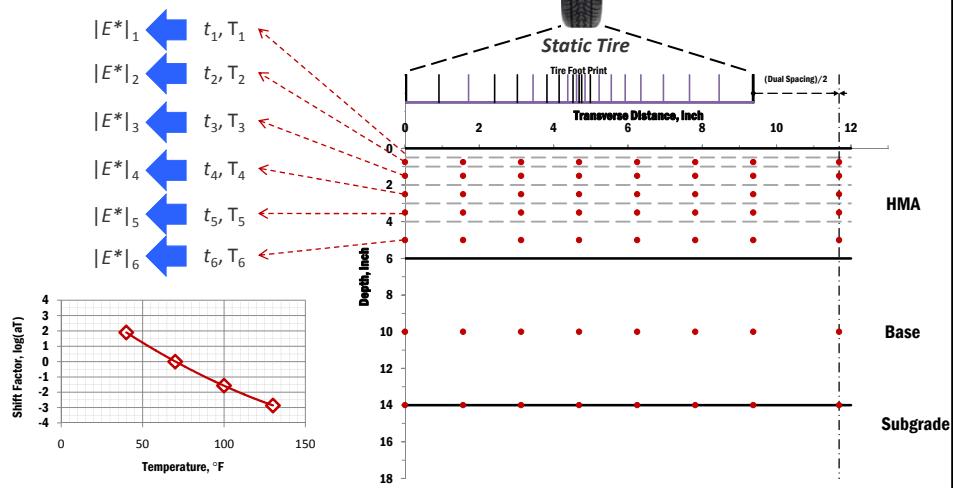
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AASHTO MEPDG Approach



Linear Elastic Analysis

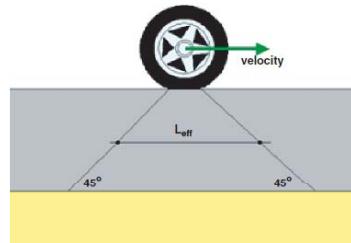


AASHTO MEPDG

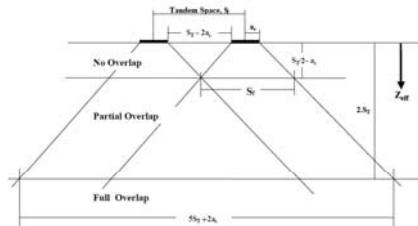


- Vertical stress distribution used to estimate traffic-induced loading time.

– Axle load configuration, Vehicle speed & Pavement structure



$$t = \frac{L_{eff}}{17.6 V_s} \quad \rightarrow \quad f = \frac{1}{t}$$



$$Z_{eff} = \sum_{i=1}^{n-1} \left(h_i \sqrt[3]{\frac{E_i}{E_{SG}}} + h_n \sqrt[3]{\frac{E_n}{E_{SG}}} \right)$$

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Literature Review



- Dongre, R. N., Myers, L. A., and D'Angelo, J. A., "Conversion of Testing Frequency to Loading Time: Impact on Performance Predictions Obtained from the Mechanistic-Empirical Pavement Design Guide", Presented at 85th Annual Meeting of the Transportation Research Board, Washington, D.C., 2006.
- Al-Qadi, I. L., W. Xie, and Elseifi, M. A., "Frequency Determination from Vehicular Loading Time Pulse to Predict Appropriate Complex Modulus in MEPDG", Journal of the Association of Asphalt Paving Technologists, Vol. 77, 2008, pp. 739-772.
- Katicha, S., Flintsch, G.W., Loulizi, A., and Wang L. "Conversion of Testing Frequency to Loading Time Applied to Mechanistic-Empirical Pavement Design Guide," Transportation Research Record No. 2087, TRB, Washington D.C., 2008, pp. 99-109.
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Appropriate Representative Elastic Modulus

B. S. Underwood and Y. R. Kim



- "Determination of the Appropriate Representative Elastic Modulus for Asphalt Concrete," IJPE, Vol. 10, Iss. 2, 2009, pp. 77-86
 - Evaluated several approximation methods for calculation of stresses & strains in linear viscoelastic materials.
 - MEPDG method is biased towards overestimating the appropriate stiffness by up to a 31% error.
 - Representative modulus to use for LEA is average of
 - dynamic modulus at a frequency equal to $1/t_p$ and
 - relaxation modulus evaluated at a time equal to $\frac{1}{2} t_p$.
 - Proposed Method resulted in 2 - 6% error

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Research Objective



- Investigate the existence of one or more *predominant frequencies (f_p)* associated with the AC layer that controls the dynamic response of pavements.
- **AC Critical Responses:**
 - Longitudinal & transverse tensile strains
 - Vertical compressive strains

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Viscoelastic vs. Pseudo Analysis



Viscoelastic



HMA $|E^*| = f(freq)$ & $\zeta = f(freq)$

CAB

SG



Pavement responses

Pseudo-dynamic



HMA

CAB

SG



Pavement responses

Pseudo-static



HMA

CAB

SG



Pavement responses

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Pavement Analysis
3D-Move Analysis Software



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Software

3D-Move

Free Softwares

3D-Move (NEW: Version 1.2) Now Available Online!

Announcement to 3D-Move Users (Posted on August 29, 2010): Inconsistency Between Text and Excel Output Files of Ver. 1.1

The last beta-version of the 3D-Move Analysis (ver 1.1) was released on July, 2010. In 3D-Move, output is provided in formats: Text and Excel. An inconsistency has inadvertently occurred when these two formats were integrated. The inconsistency was present only in the Excel file, while the Text file output is correct. The origin of the slip-up was traced to the allocation of the columns when the data sharing between Text and Excel output files occurred. Further, there were concerns about the units of the 3D-Move responses being not prominently displayed. These issues have been corrected and a modified beta-version of 3D-Move (ver 1.2) is now available for download.

Announcements

DISCUSSION GROUP* at 3d-move.lmdiscussion.com to provide your feedback or post your questions on the 3D-Move Analysis Software.

Freeware Download at:
<http://www.arc.unr.edu/Software.html>

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Pavement Analysis
3D-Move Analysis Software - Validation



1. 3D-Move vs. ViscoRoute (2010)

- ViscoRoute (IFFSTAR – LCPC): moving circular loaded areas with uniform contact pressure, viscoelastic material properties

Reference:

Chabot, A., Chupin, O., Deloffre, L., and Duhamel, D., "Viscoroute 2.0: a tool for the simulation of moving load effects on asphalt pavement," Road Materials and Pavement Design an International Journal, Volume 11/2, 2010, pp. 227-250.

Loft A., "Evaluation de Viscoroute-v1 pour l'étude de quelques chaussées souples". Msc. Dissertation, Dresden University of Technology speciality Urban and Road construction, 2005.

$\epsilon_{yy} \cdot 10^{-6}$

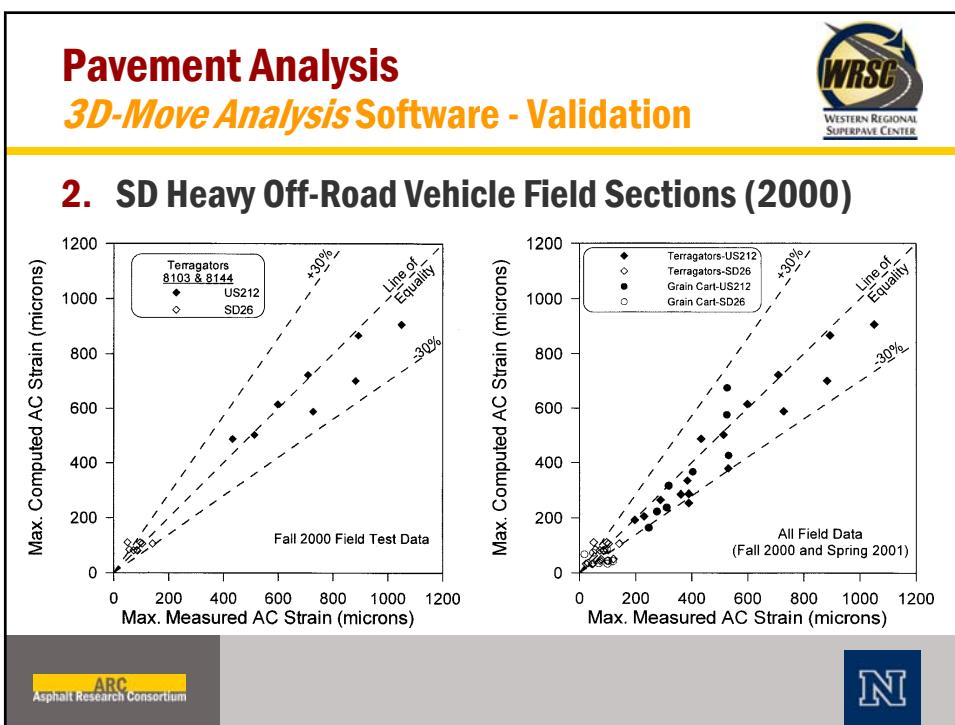
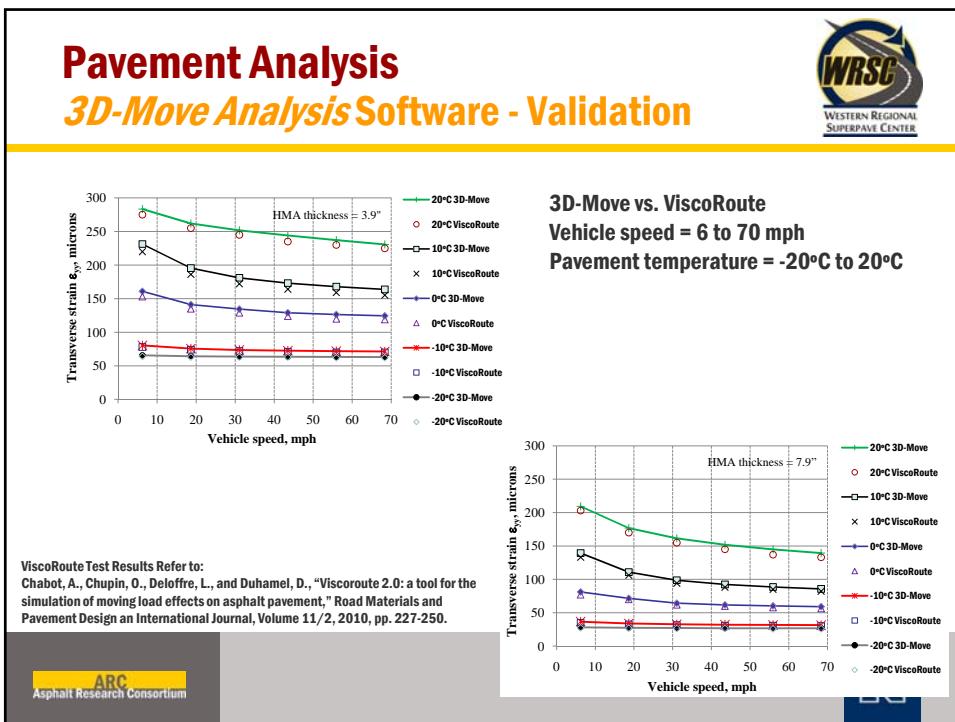
t (s)

A380 Pavement Experimental Program for aircrafts.

Viscoelastic calculus
Strain gages
Elastic calculus

Comparison between elastic computations, ViscoRoute1.0 simulations and transversal strain measurements at the bottom of bituminous layers for a 4-wheels moving load

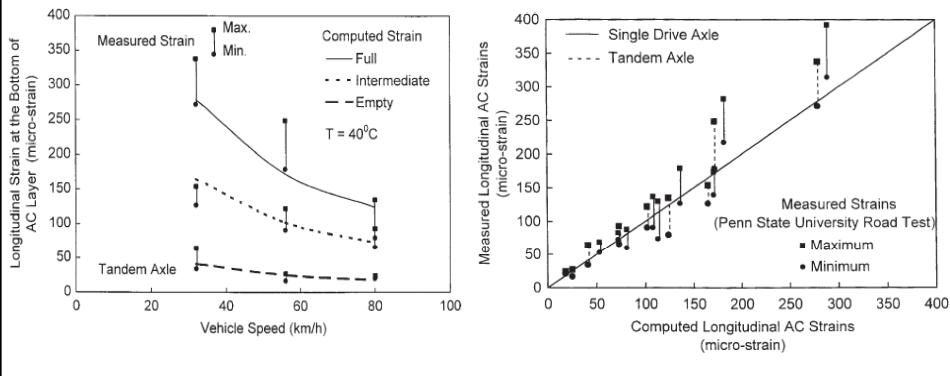
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Pavement Analysis 3D-Move Analysis Software - Validation



3. PennState University Test Track (1999)



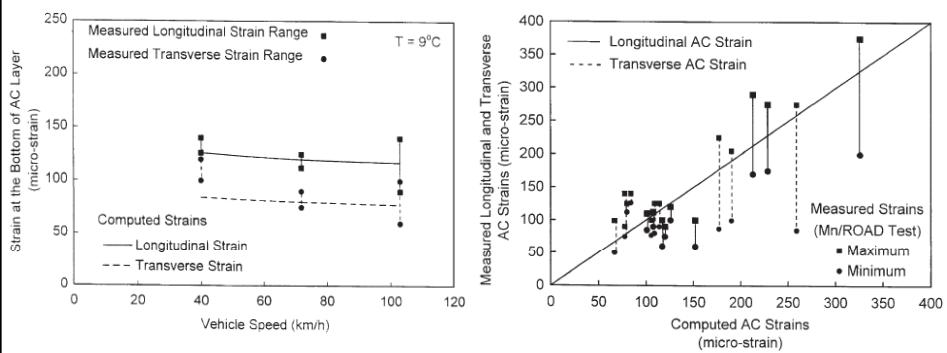
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Pavement Analysis 3D-Move Analysis Software - Validation



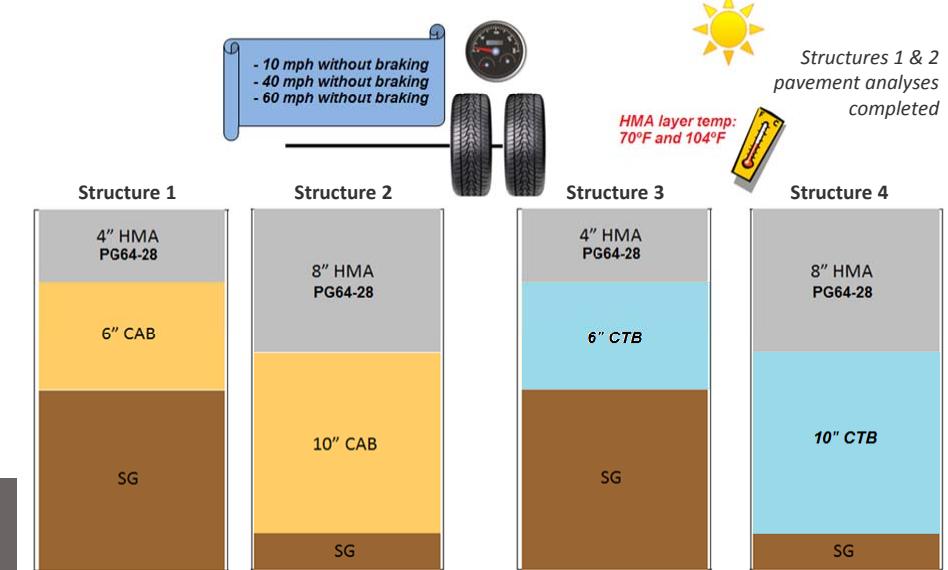
4. MnRoad (1997)



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Database of pavement responses



Pavement Responses Locations



4 inch HMA layer

0.25"	X	X	X	X	X
0.5"	X	X	X	X	X
0.75"	X	X	X	X	X
1.5"	X	X	X	X	X
2.5"	X	X	X	X	X
3.5"	X	X	X	X	X
4.0"	X	X	X	X	X

8 inch HMA layer

0.5"	X	X	X	X	X
0.5"	X	X	X	X	X
0.75"	X	X	X	X	X
1.5"	X	X	X	X	X
2.5"	X	X	X	X	X
3.5"	X	X	X	X	X
6.0"	X	X	X	X	X
8.0"	X	X	X	X	X



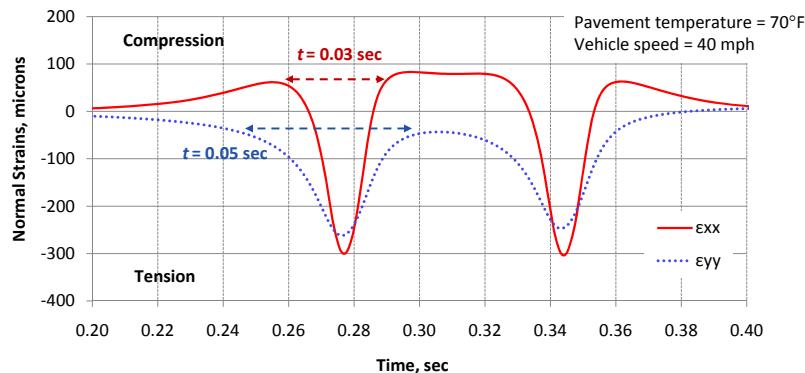
Data analysis completed for responses at center line of the load



Proposed approach to determine f_p



- Example: Bottom of the 4-inch HMA layer:



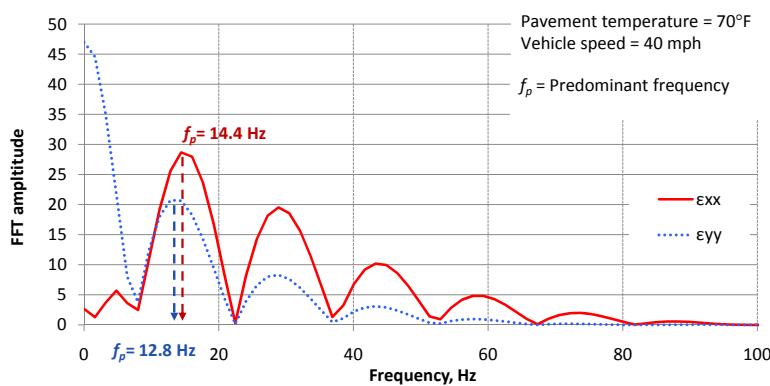
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Proposed approach to determine f_p



- FFT amplitudes of the normal strains of the 4-inch HMA



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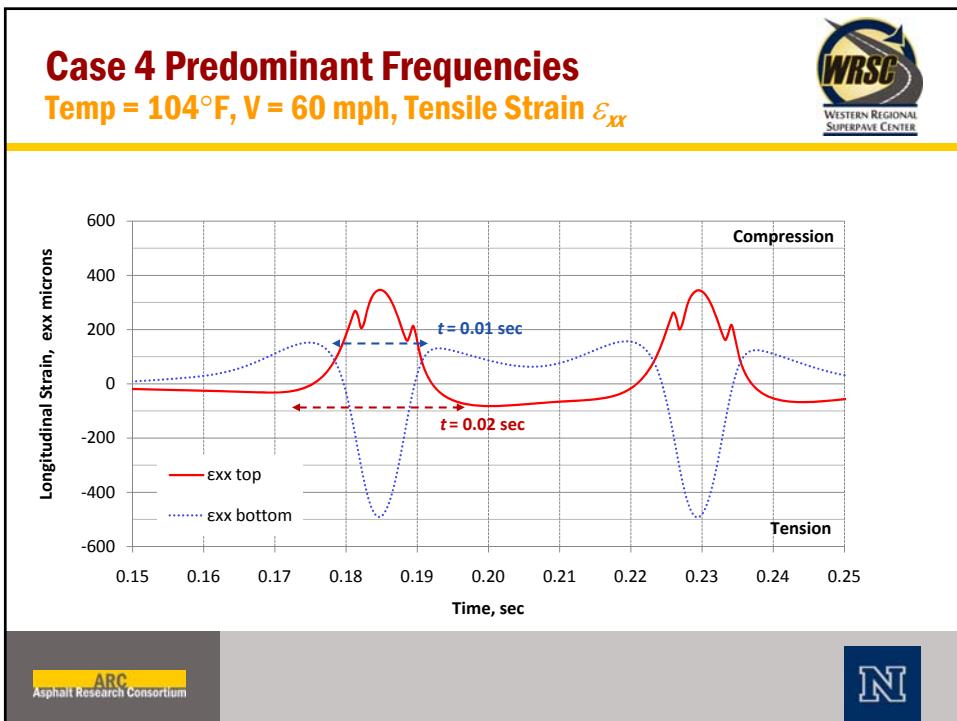
***f_p* for the 4-inch HMA layer**

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Case Study	Depth (in)	Predominant frequency, (Hz)							
		ϵ_{xx}	$f_{p,xx}$	ϵ_y	$f_{p,y}$	ϵ_x	$f_{p,x}$	σ_{xz}	$f_{p,z}$
Case 1: 70°F and 40 mph	0.25	14.4		12.8		14.4		14.4	
	0.5	14.4		12.8		14.4		14.4	
	0.75	14.4		12.8		14.4		14.4	
	1.5	14.4	14.4	12.8	14.4	14.4	14.4	14.4	14.4
	2.5	14.4		12.8		14.4		14.4	
	3.5	14.4		12.8		14.4		14.4	
Case 2: 104°F and 40 mph	0.25	14.4		14.4		14.4		14.4	
	0.5	14.4		12.8		30.4		14.4	
	0.75	14.4		14.4		30.4		14.4	
	1.5	12.8		14.4	14.4	30.4		14.4	
	2.5	30.4		30.4		14.4		14.4	
	3.5	30.4		14.4		14.4		14.4	
Case 3: 70°F and 60 mph	4	28.8		14.4		14.4		14.4	
	0.25	21.6		19.4		21.6		21.6	
	0.5	21.6		19.4		21.6		21.6	
	0.75	21.6		19.4		21.6		21.6	
	1.5	21.6	21.6	16.8	21.6	21.6	21.6	21.6	21.6
	2.5	21.6		21.6		21.6		21.6	
Case 4: 104°F and 60 mph	3.5	21.6		19.4		21.6		21.6	
	4	30.4		19.4		31.6		31.6	
	0.25	21.6		21.6		43.3		21.6	
	0.5	21.6		19.2		43.3		21.6	
	0.75	21.6		19.2		43.3		21.6	
	1.5	21.6		21.6		43.3		21.6	
Case 5: 70°F and 10 mph	2.5	43.3		21.6		21.6		21.6	
	3.5	43.3	43.3	21.6		21.6		21.6	
	4	43.3		21.6		21.6		21.6	
	0.25	21.6		21.6		3.6		3.6	
	0.5	3.6		3.2		3.6		3.6	
	0.75	3.6		3.2		3.6		3.6	
Case 6: 104°F and 10 mph	1.5	3.2		3.2		7.6		3.6	
	2.5	7.6		3.2		7.6		3.6	
	3.5	4		3.6		7.6		3.6	
	4	4		3.6		3.6		3.6	
	0.25	7.6		3.2		7.6		3.6	
	0.5	7.6	7.6	3.2		7.6		3.6	

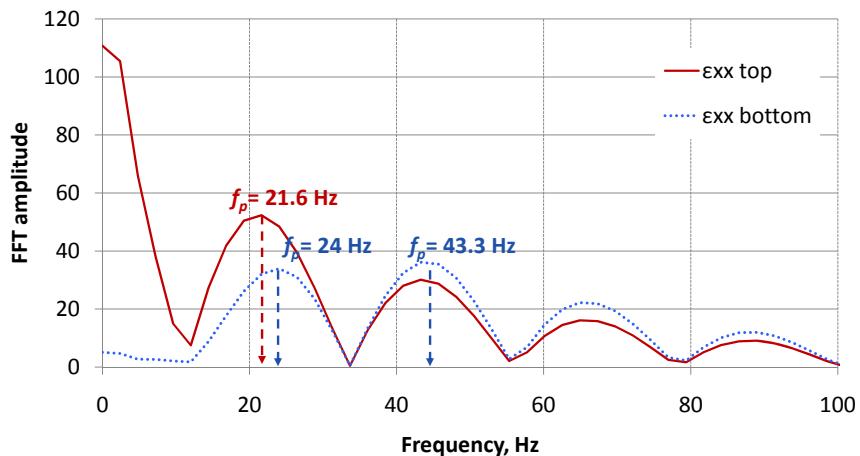
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Case 4 Predominant Frequencies

Temp = 104°F, V = 60 mph, Tensile Strain ε_{xx}



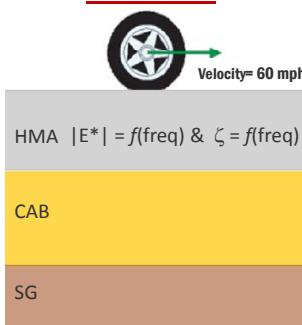
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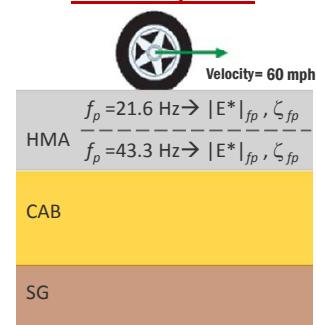
Pseudo-Dynamic Analysis



Viscoelastic



Pseudo-dynamic



Pavement responses \longleftrightarrow *Pavement responses*

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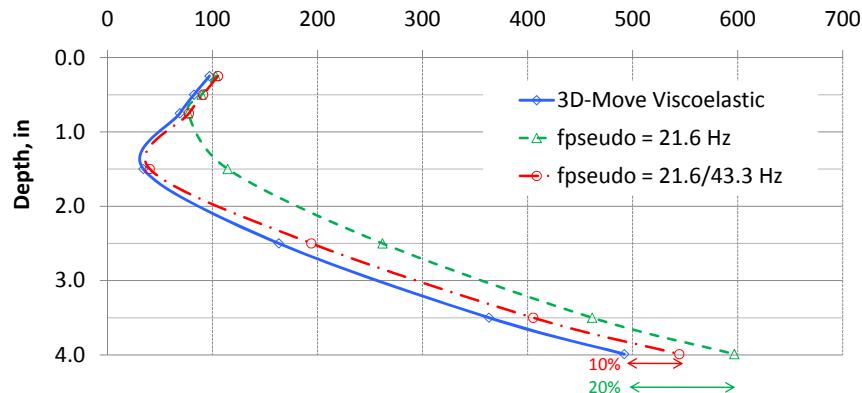
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Case 4 Pseudo-Dynamic Analysis

Temp = 104°F, V = 60 mph, Tensile Strain ϵ_{xx}



Maximum tensile strain ϵ_{xx} , microns



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f_p for the 8-inch HMA layer



Case Study	Depth* (in)	Predominant frequency, (Hz)							
		ϵ_{xx} f_p visco	ϵ_{yy} f_p visco	ϵ_{zz} f_p visco	σ_{xx} f_p visco	σ_{yy} f_p visco	σ_{zz} f_p visco	ϵ_{xx} f_p pseudo	ϵ_{yy} f_p pseudo
Case 7: 70°F and 40 mph	0.25	12.8	16	30.4	14.4	14.4	14.4	14.4	14.4
	0.5	12.8	11.2	30.4	14.4	14.4	14.4	14.4	14.4
	0.75	12.8	9.6	30.4	14.4	14.4	14.4	14.4	14.4
	1.0	12.8	14.4	30.4	14.4	14.4	14.4	14.4	14.4
	1.5	12.8	14.4	30.4	14.4	14.4	14.4	14.4	14.4
	2.5	12.8	14.4	30.4	14.4	14.4	14.4	14.4	14.4
	3.5	30.4	14.4	30.4	14.4	14.4	14.4	14.4	14.4
	6	30.4	12.8	12.8	12.8	12.8	12.8	12.8	12.8
Case 8: 104°F and 40 mph	0.25	14.4	12.8	30.4	14.4	14.4	14.4	14.4	14.4
	0.5	14.4	12.8	30.4	14.4	14.4	14.4	14.4	14.4
	0.75	14.4	11.2	30.4	14.4	14.4	14.4	14.4	14.4
	1.0	12.8	12.8	30.4	14.4	14.4	14.4	14.4	14.4
	1.5	30.4	12.8	14.4	14.4	14.4	14.4	14.4	14.4
	2.5	30.4	12.8	14.4	14.4	14.4	14.4	14.4	14.4
	3.5	30.4	12.8	14.4	14.4	14.4	14.4	14.4	14.4
	6	30.4	12.8	14.4	14.4	14.4	14.4	14.4	14.4
Case 9: 70°F and 60 mph	0.25	19.2	19.2	19.2	21.6	21.6	21.6	21.6	21.6
	0.5	19.2	16.8	40.8	21.6	21.6	21.6	21.6	21.6
	0.75	19.2	16.8	45.7	21.6	21.6	21.6	21.6	21.6
	1.0	19.2	19.2	45.7	21.6	21.6	21.6	21.6	21.6
	1.5	19.2	19.2	21.6	21.6	21.6	21.6	21.6	21.6
	2.5	45.7	21.6	19.2	21.6	21.6	21.6	21.6	21.6
	3.5	45.7	21.6	19.2	21.6	21.6	21.6	21.6	21.6
	6	45.7	19.2	19.2	21.6	21.6	21.6	21.6	21.6
Case 10: 104°F and 60 mph	0.25	21.6	19.2	45.7	21.6	21.6	21.6	21.6	21.6
	0.5	21.6	19.2	45.7	21.6	21.6	21.6	21.6	21.6
	0.75	21.6	16.8	45.7	21.6	21.6	21.6	21.6	21.6
	1.0	21.6	21.6	21.6	21.6	21.6	21.6	21.6	21.6
	1.5	45.7	21.6	21.6	21.6	21.6	21.6	21.6	21.6
	2.5	45.7	21.6	21.6	21.6	21.6	21.6	21.6	21.6
	3.5	45.7	21.6	21.6	21.6	21.6	21.6	21.6	21.6
	6	43.3	21.6	21.6	21.6	21.6	21.6	21.6	21.6
Case 11: 70°F and 10 mph	0.25	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.5	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.75	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	1.0	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	1.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	2.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	3.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	6	3.6	3.2	3.6	3.6	3.6	3.6	3.6	3.6
Case 12: 104°F and 10 mph	0.25	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.5	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.75	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	1.0	11.2	7.6	3.6	3.6	3.6	3.6	3.6	3.6
	1.5	11.2	7.6	3.6	3.6	3.6	3.6	3.6	3.6
	2.5	11.2	7.6	3.6	3.6	3.6	3.6	3.6	3.6
	3.5	11.2	7.6	3.6	3.6	3.6	3.6	3.6	3.6
	6	4	3.2	3.6	3.6	3.6	3.6	3.6	3.6
Case 13: 104°F and 10 mph	0.25	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.5	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.75	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	1.0	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	1.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	2.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	3.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	6	3.6	3.2	3.6	3.6	3.6	3.6	3.6	3.6
Case 14: 104°F and 10 mph	0.25	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.5	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.75	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	1.0	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	1.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	2.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	3.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	6	3.6	3.2	3.6	3.6	3.6	3.6	3.6	3.6
Case 15: 104°F and 10 mph	0.25	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.5	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	0.75	3.6	3.2	7.6	3.6	3.6	3.6	3.6	3.6
	1.0	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	1.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	2.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	3.5	3.6	3.6	7.6	3.6	3.6	3.6	3.6	3.6
	6	3.6	3.2	3.6	3.6	3.6	3.6	3.6	3.6

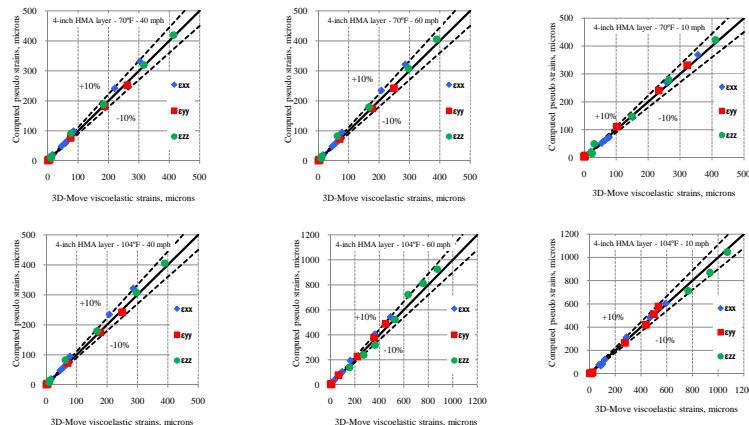
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Viscoelastic vs. Pseudo-Dynamic analysis



4-inch HMA layer



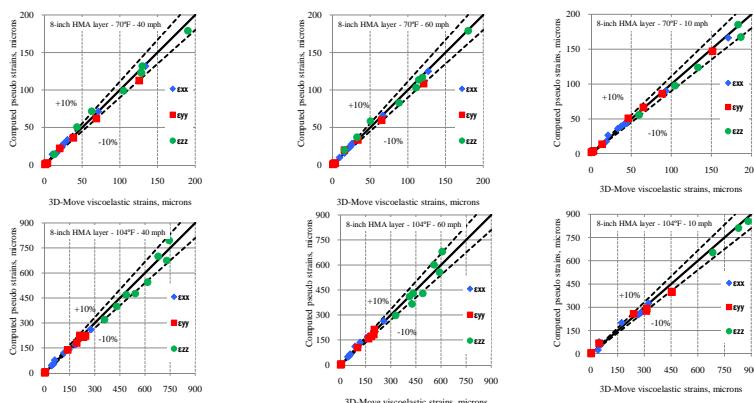
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Viscoelastic vs. Pseudo-Dynamic analysis



8-inch HMA layer



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Pseudo-Static Analysis

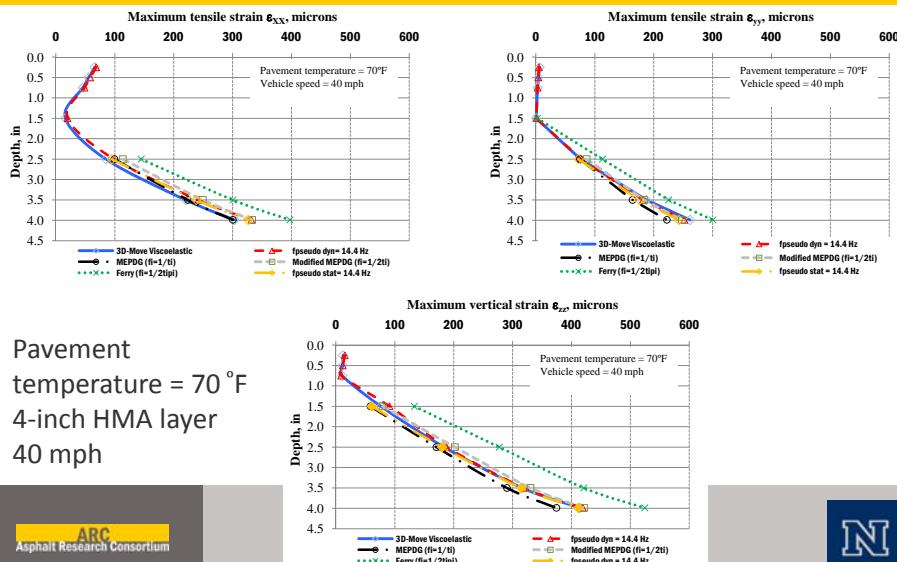


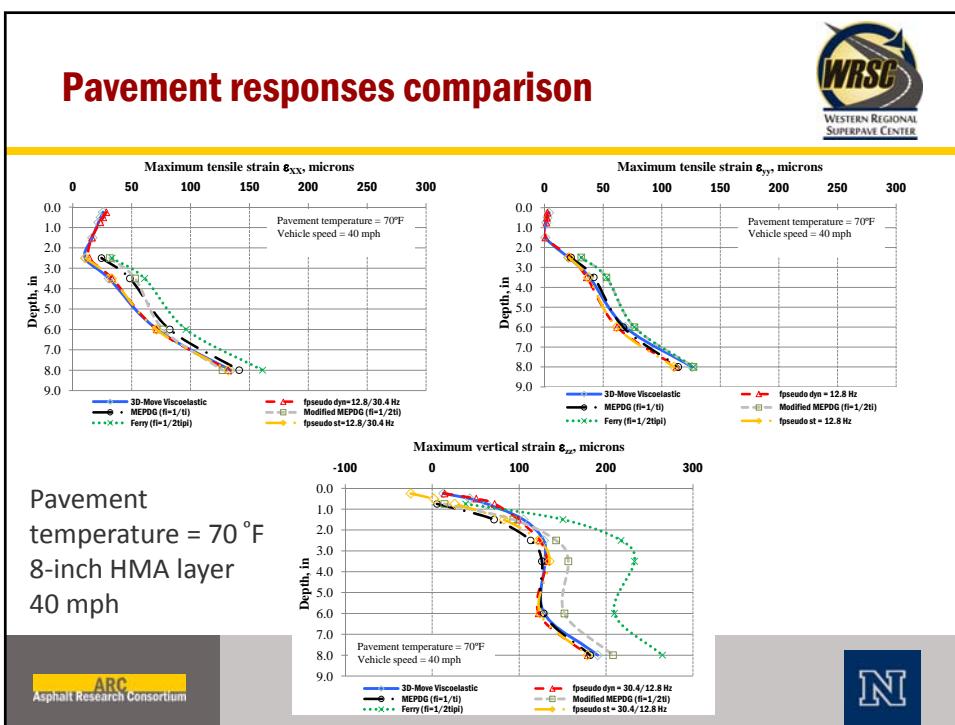
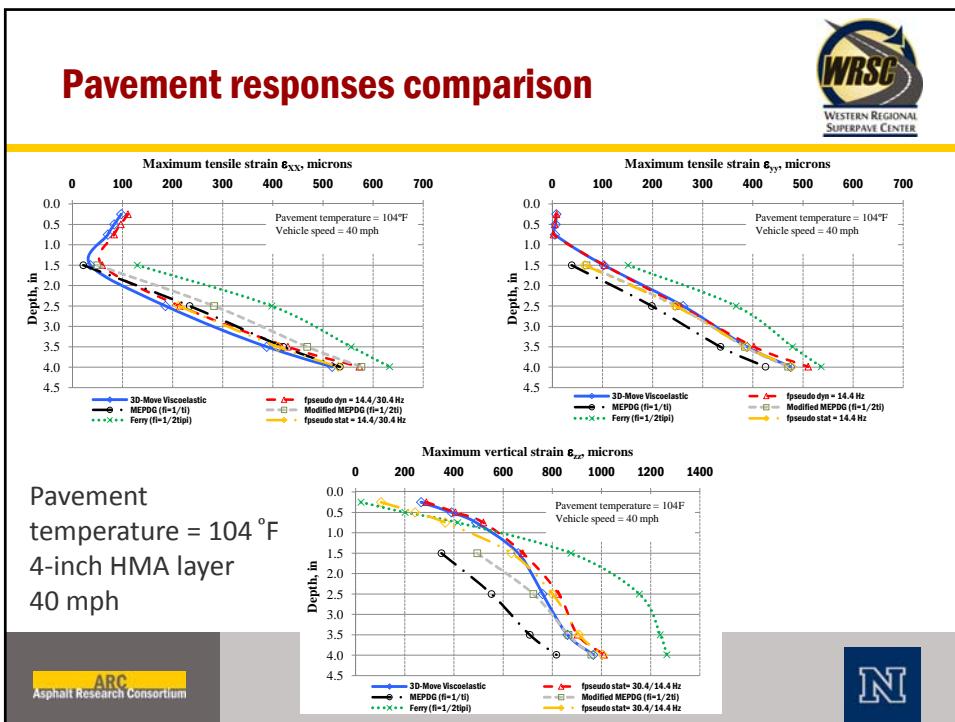
- Pseudo-Static:
 - Vehicle speed = 0
 - Linear Elastic Analysis (LEA)
 - Use f_p to select $|E^*|_{fp}$
 - Damping $\zeta_{fp} = 0$
- Also Compare pavement responses following
 - MEPDG approach ($f = 1/t$)
 - Modified MEPDG ($f = 1/(2t)$)
 - Ferry ($f = 1/(2\pi t)$)

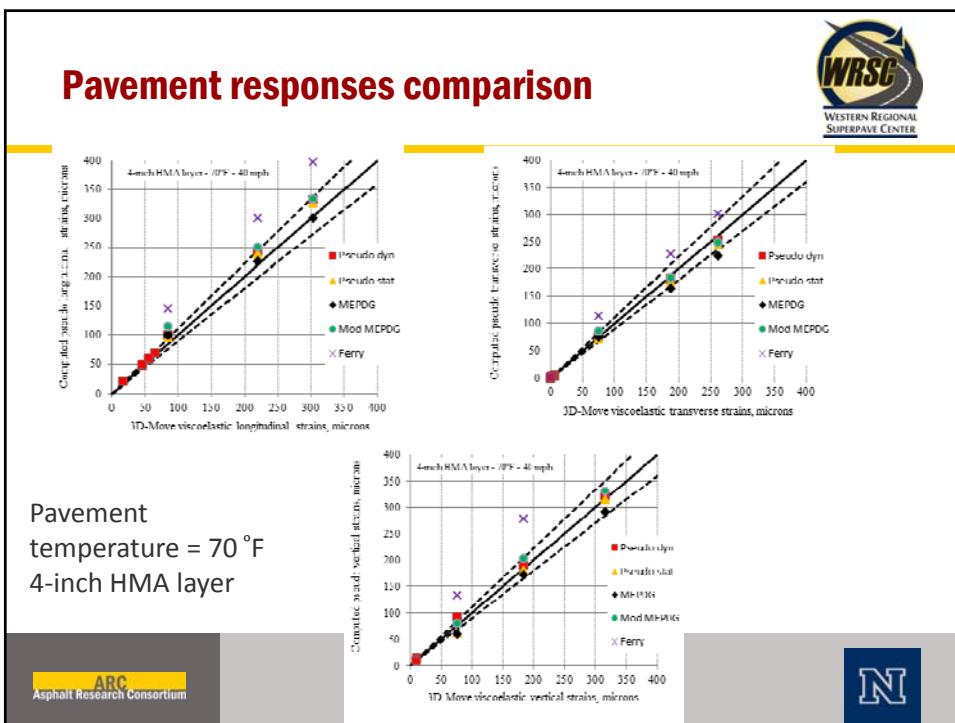
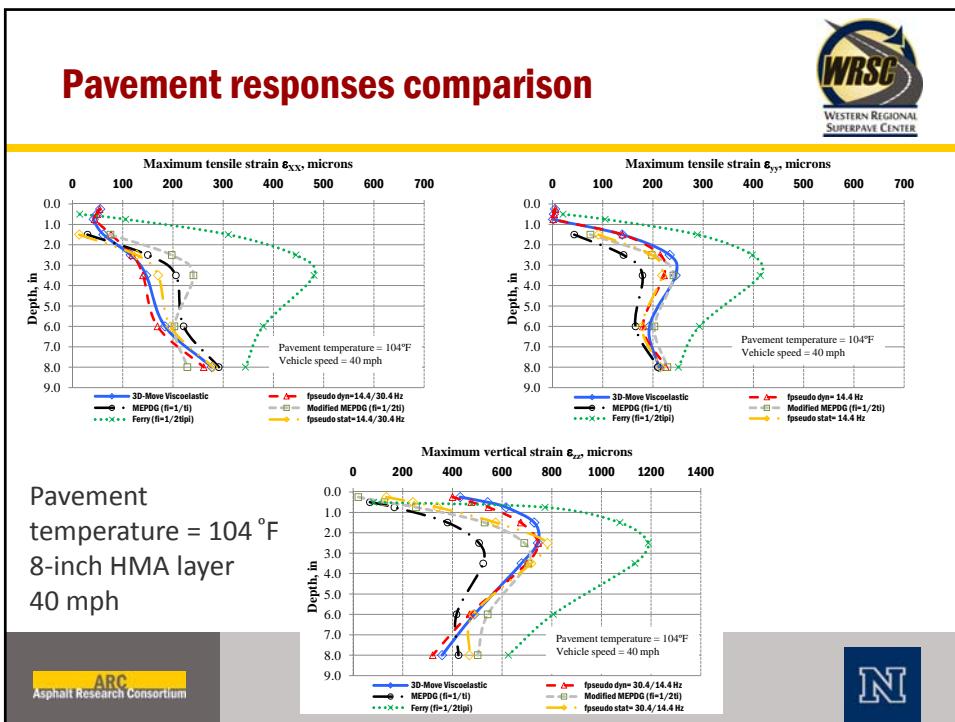
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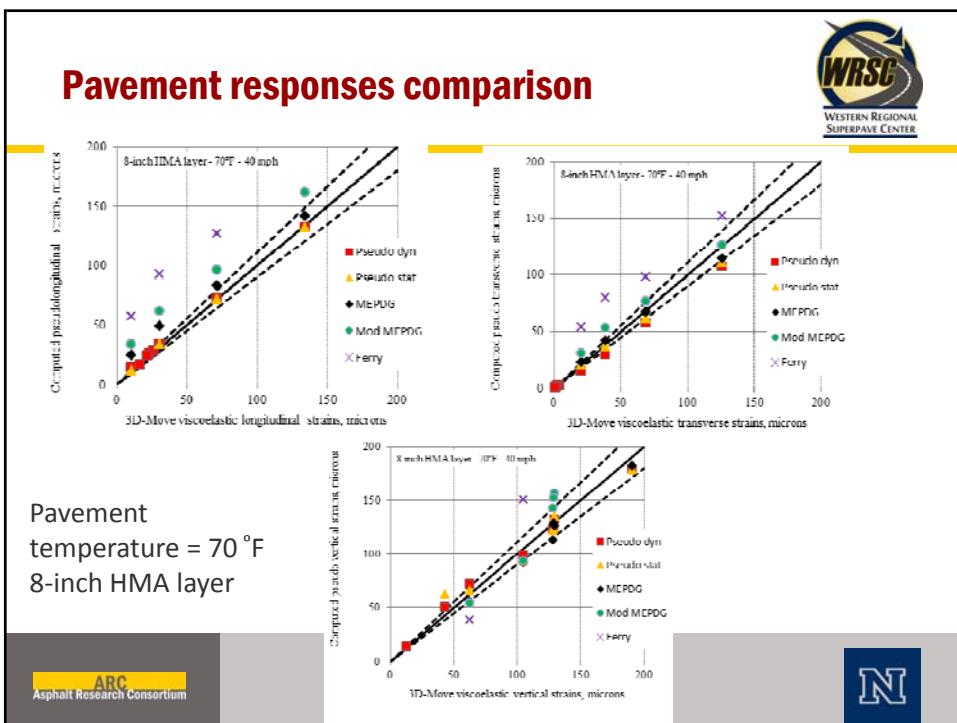
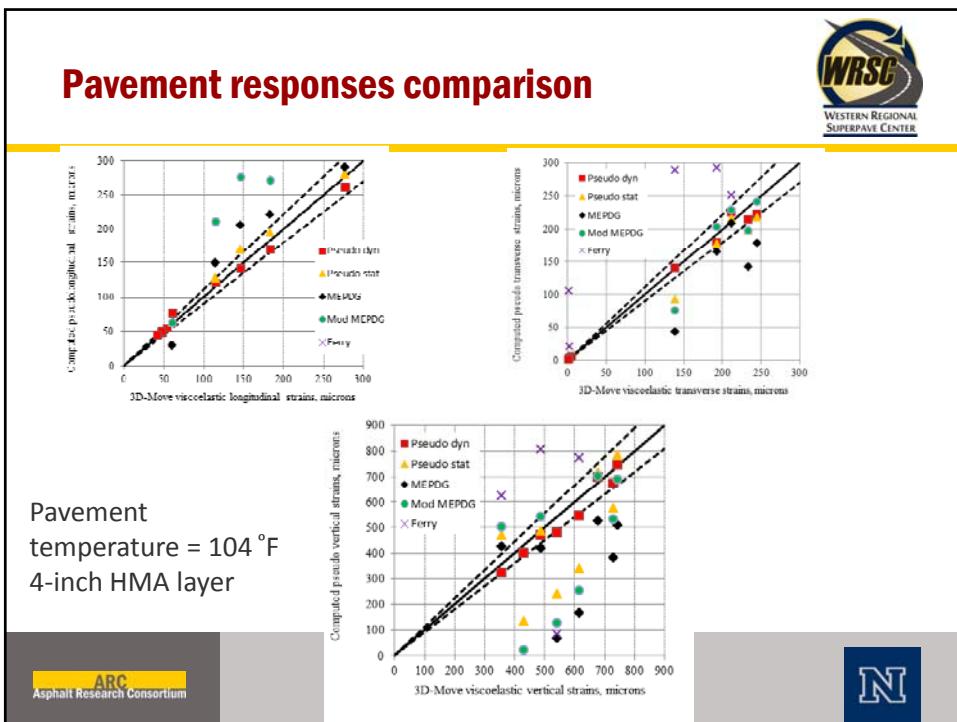
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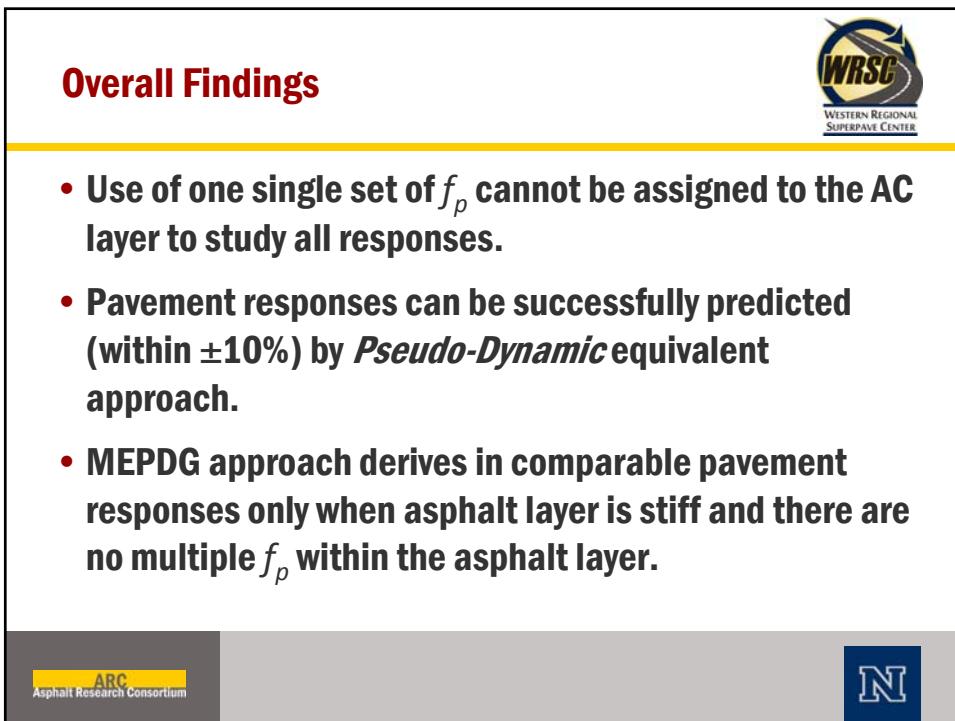
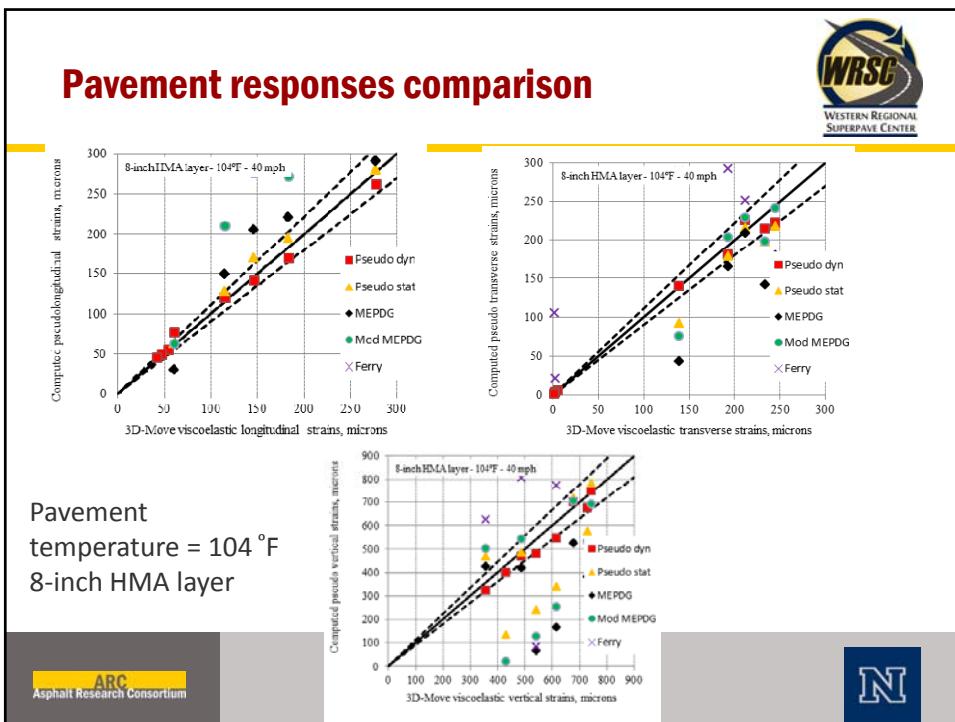
Pavement responses comparison











Additional needed work...



- Investigate influence of axle load, response location and axle configuration on f_p .
- Investigate influence of CTB on f_p .
- Evaluate different time-frequency conversions.
- Other!

...Feedback...

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- Contents reflect the views of the authors and do not necessarily reflect the official views & policies of FHWA.

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