



University of Nevada, Reno



# Performance Evaluation of Asphalt Mixtures With High RAP Content

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WESTERN REGIONAL SUPERPAVE CENTER



## OVERALL OBJECTIVES

- Can current *design techniques* be used to design high RAP contents HMA mixes?
- Validation of existing and new procedures for *characterizing RAP materials*.
- Side-by-side comparison of *field performance* for HMA w/o and HMA with high RAP.
- Can laboratory-produced mixtures' properties be used to *ensure quality field-produced mixtures*?



## PTH-8 RAP PROJECT LAYOUT

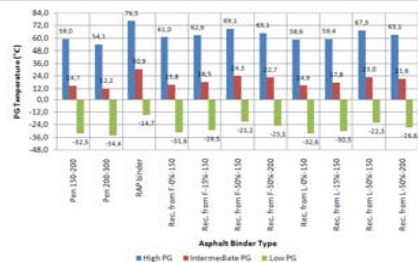
~1.5 miles	~1.5 miles	~1.5 miles	~1.5 miles
4 <sup>th</sup> lift: HMA / 50% RAP	HMA / 50% RAP w/ grade change	HMA / 15% RAP	HMA / No RAP
3 <sup>rd</sup> lift: HMA / 50% RAP	HMA / 50% RAP w/ grade change	HMA / 15% RAP	HMA / No RAP
2 <sup>nd</sup> lift: HMA / 50% RAP			
1 <sup>st</sup> lift: HMA / 50% RAP			

## EXPERIMENTAL PLAN

- Evaluation of *field-produced* and *laboratory-produced* HMA mixtures with 0, 15 and 50% RAP content from field sections in *Manitoba-Canada*.
- Evaluation of the applicability of the blending chart process to predict the PG of the blended asphalt binder.
- Comparison between the properties and performance of the field- and laboratory-produced mixtures

Property	F-0%-150	F-15%-150	F-50%-150	F-50%-200	L-0%-150	L-15%-150	L-50%-150	L-50%-200
AASHTO T283 at multiple F-T	X	X	X	X	X	X	X	X
TS vs. F-T cycles: 0, 1 and 3 F-T	X	X	X	X	X	X	X	X
TSR at 1 and 3 F-T	X	X	X	X	X	X	X	X
Modulus at multiple F-T	X	X	X	X	X	X	X	X
E*  vs. F-T cycles: 0, 1 and 3 F-T	X	X	X	X	X	X	X	X
Resistance to thermal cracking	X	X	X	X	X	X	X	X
TSRT: 0 and 3 F-T	X	X	X	X	X	X	X	X

## ASPHALT BINDERS TRUE GRADES



## ASPHALT BINDERS PG GRADES

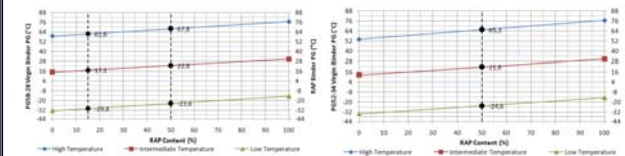
Binder	PG Grade
Pen 150-200	58-28
Pen 200-300	52-34
RAP Binder	76-10
Recovered from F-0%-150	58-28
Recovered from F-15%-150	58-28
Recovered from F-50%-150	64-16
Recovered from F-50%-200	64-22
Recovered from L-0%-150	58-28
Recovered from L-15%-150	58-28
Recovered from L-50%-150	64-22
Recovered from L-50%-200	58-22

## BLENDING CHARTS

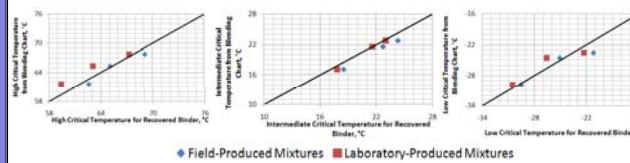
$$T_{virgin} = \frac{T_{blend} - (\%RAP \text{ binder} \times T_{RAP})}{(1 - \%RAP \text{ binder})}$$

where:  $T_{blend}$  = critical temperature of blended asphalt binder  
 $T_{virgin}$  = critical temperature of virgin asphalt binder  
 $T_{RAP}$  = critical temperature of recovered RAP binder  
 $\%RAP \text{ binder}$  = percent RAP binder in the RAP expressed as a decimal

### Blending Chart process for PG58-28 and PG52-34

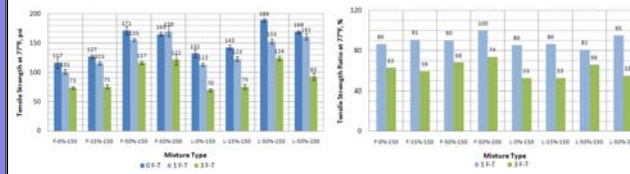
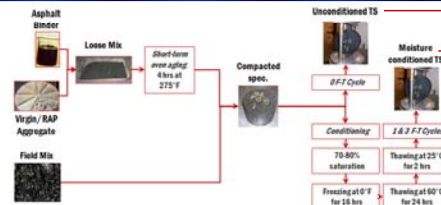


### Estimated vs. measured Critical Temperatures



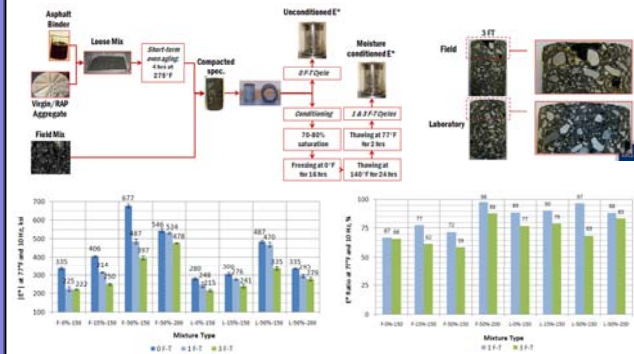
## LABORATORY EVALUATION

### TS and TSR at Multiple F-T Cycles

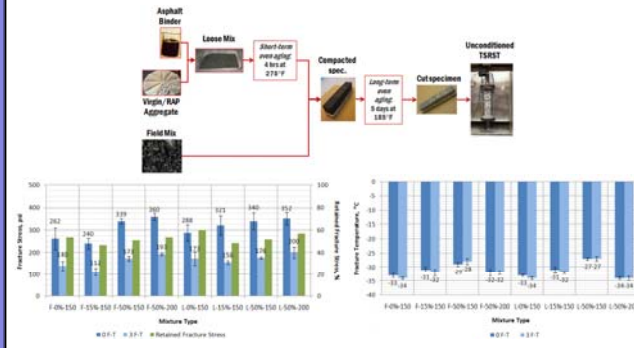


## LABORATORY EVALUATION (cont...)

### Dynamic Modulus (|E\*|) at Multiple F-T Cycles



### Thermal Cracking Resistance at Multiple F-T Cycles



## FINDINGS AND CONCLUSIONS

- Good correlations were observed between estimated critical temperatures from the blending chart and measured ones from recovered asphalt binders.
- The use of multiple F-T cycles provided a better characterization of the mixtures resistance to moisture damage.
- Higher or similar TS were observed for the laboratory-produced mixtures when compared to the field-produced mixtures.
- Field-produced and laboratory-produced mixtures ranked similarly in the AASHTO T283, |E\*| and TSRST tests.

## ACKNOWLEDGMENT

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