



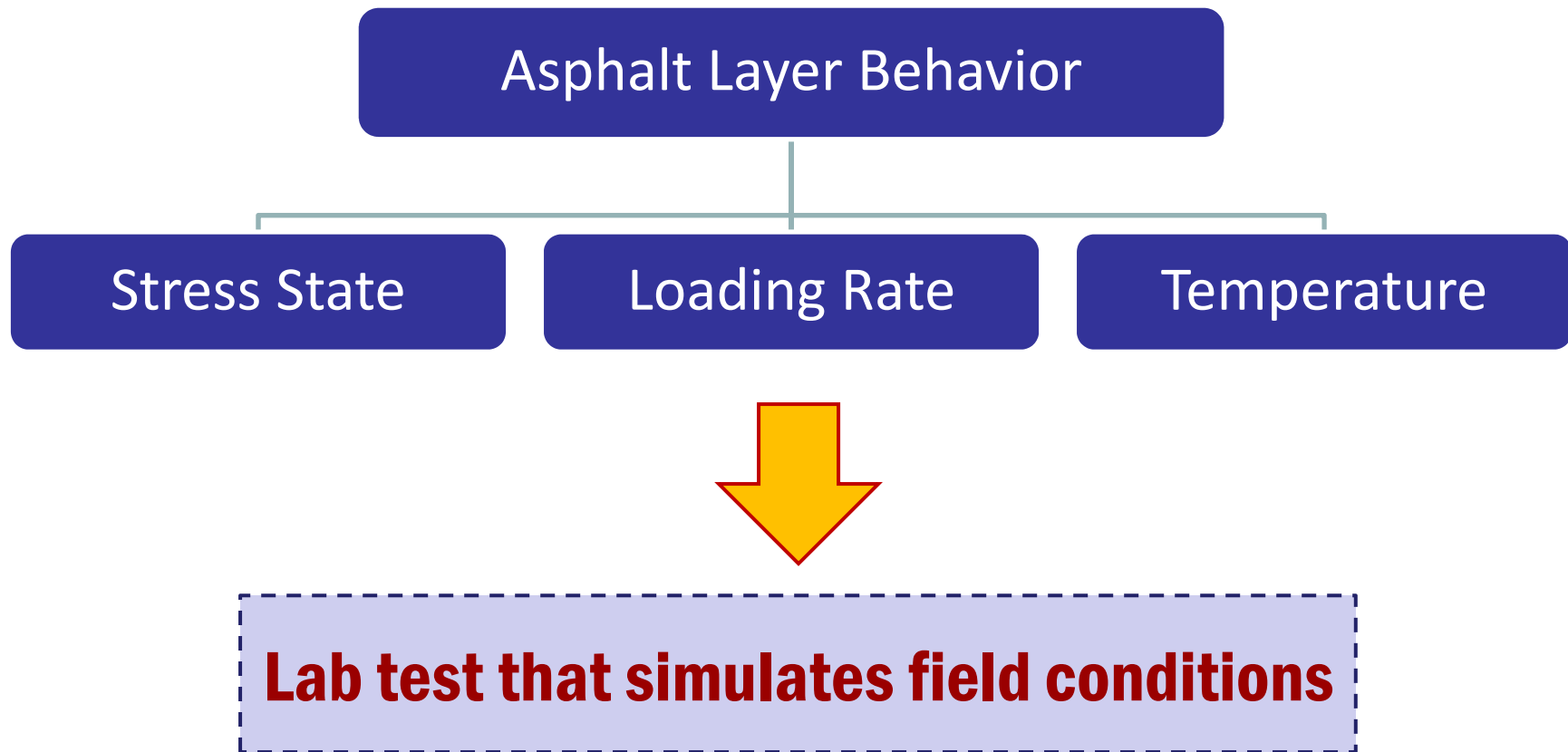
# **Characteristics of the Loading Pulse for the Flow Number Performance Test**

**Elie Y. Hajj, Alvaro Ulloa, Raj Siddharthan, Peter E. Sebaaly**

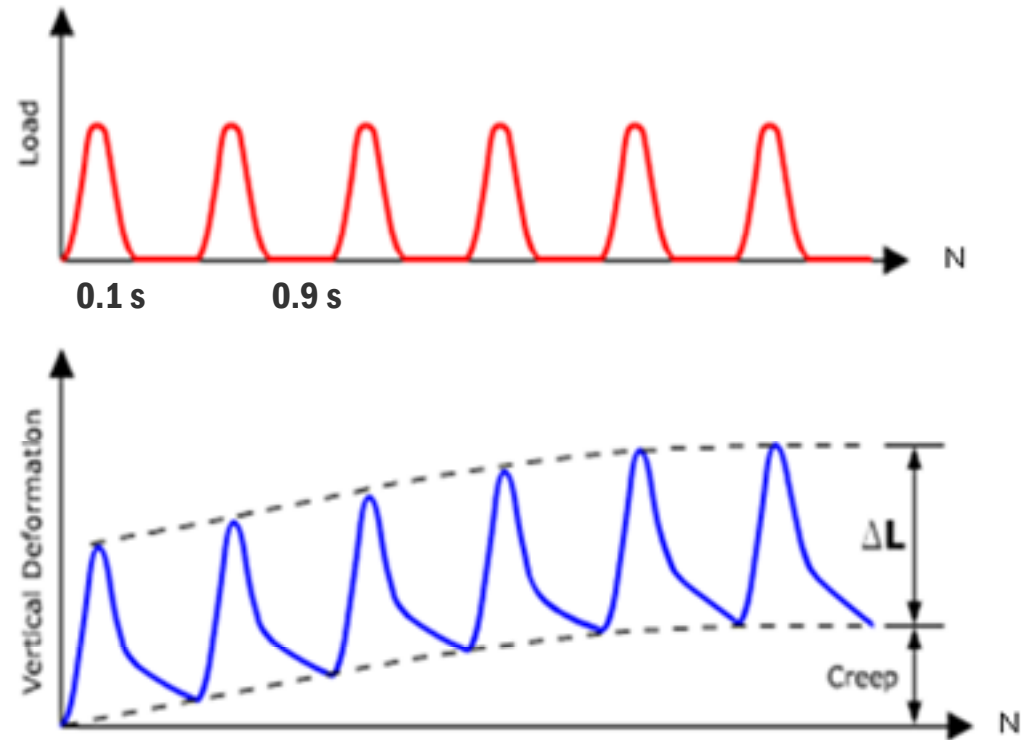
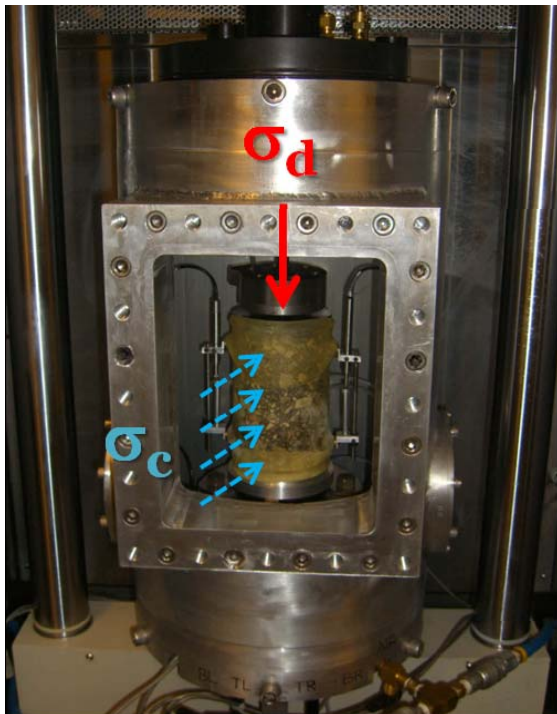
***Association of Asphalt Paving Technologists Annual Meeting  
March 7-10, 2010, Sacramento, California***

# Introduction

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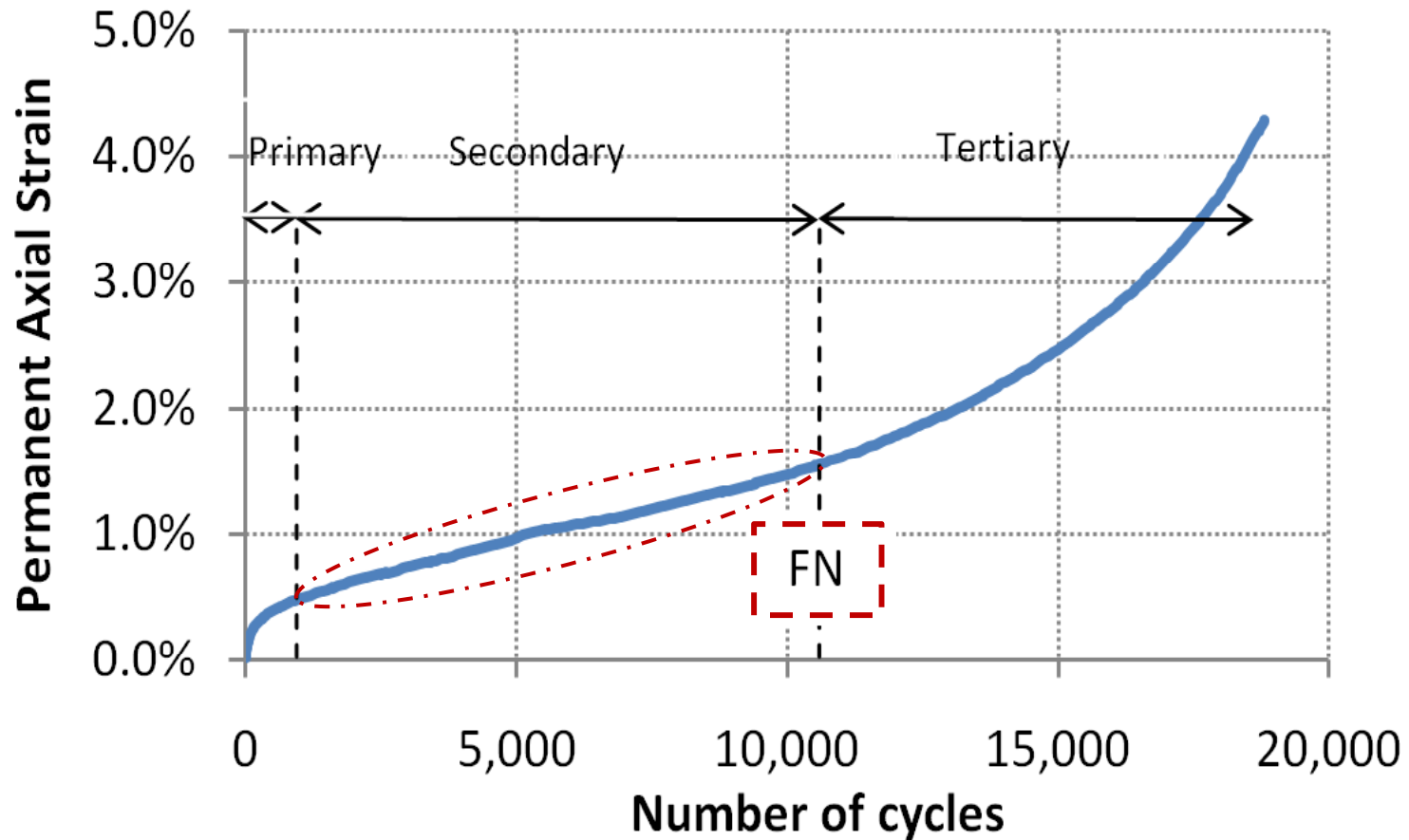


# Flow number (FN) test

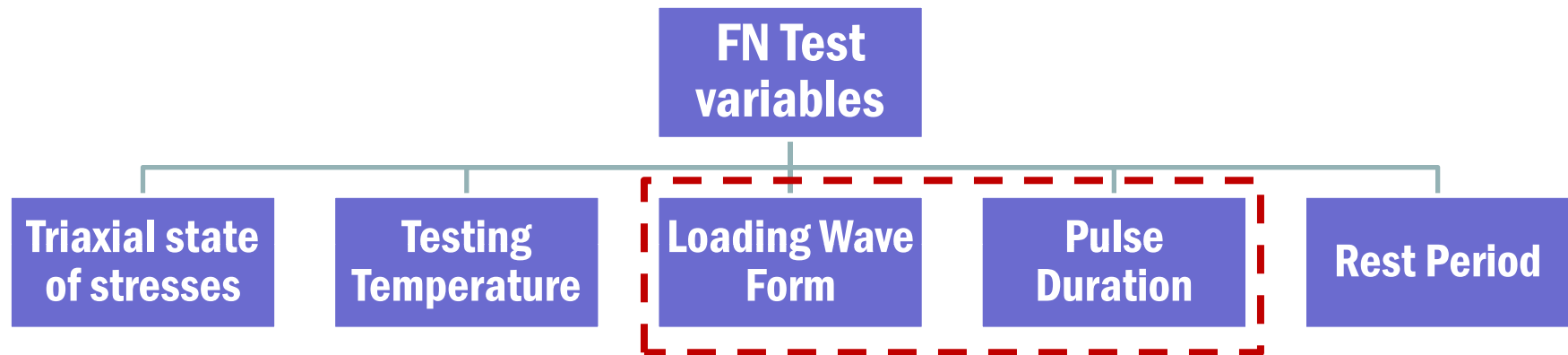


# Flow number (FN) test

## Permanent deformation Characterization



# Objective

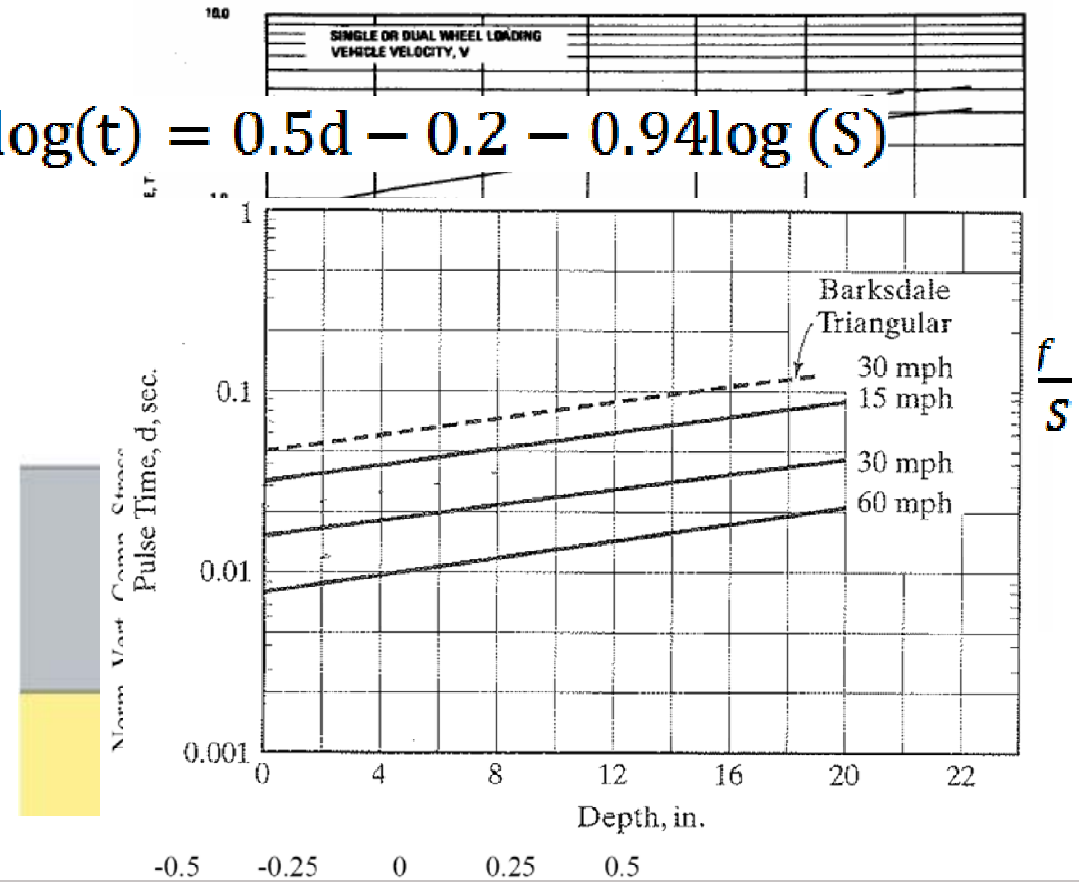


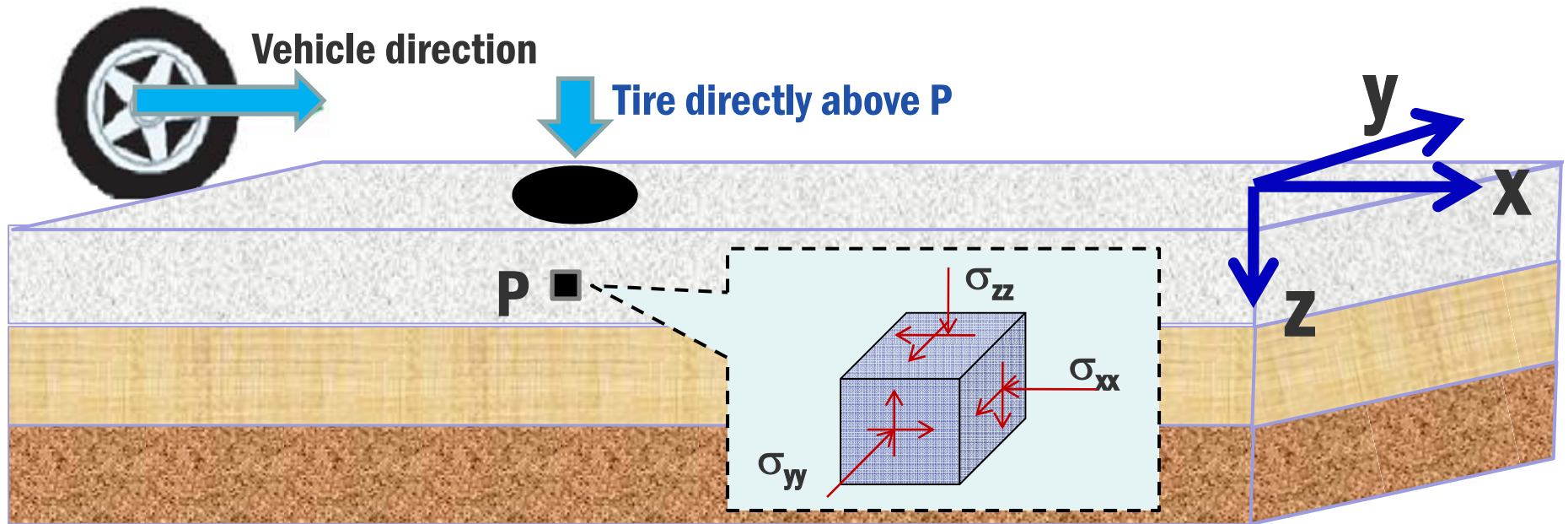
**Provide recommendations for the characteristics of the deviator loading pulse in the flow number test**

# Pulse duration prediction

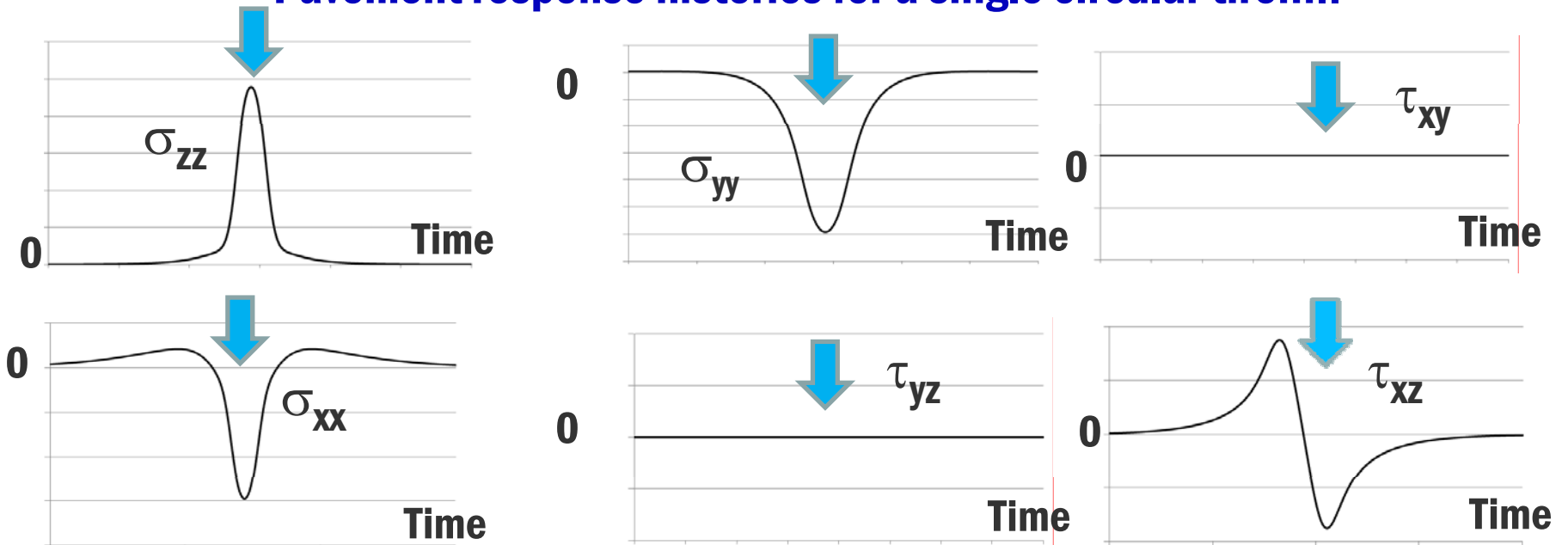
- ▣ Barksdale, 1971
- ▣ Brown, 1973 →
- ▣ McLean, 1974
- ▣ MEPDG, 2002
- ▣ Al-Qadi, 2008
- ▣ ...

$$\log(t) = 0.5d - 0.2 - 0.94\log(S)$$



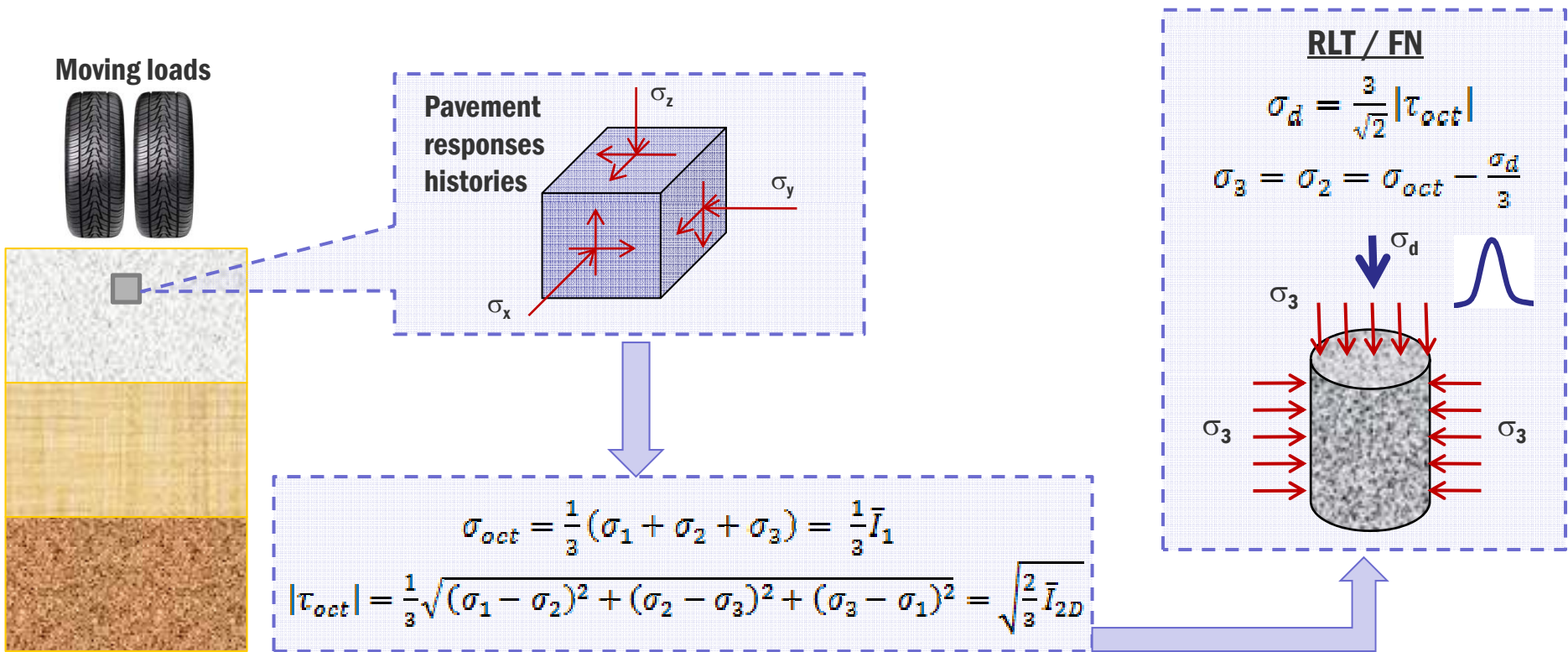


**Pavement response histories for a single circular tire.....**



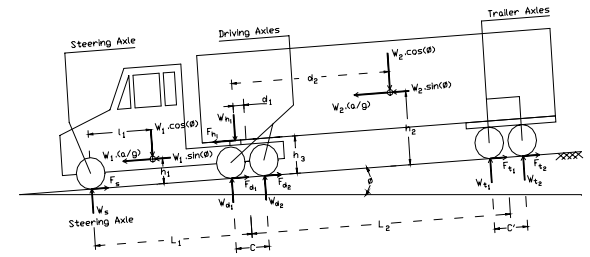
**Question: What stress pulse shape to use in triaxial test?**

# Stress State in the Triaxial FN Test





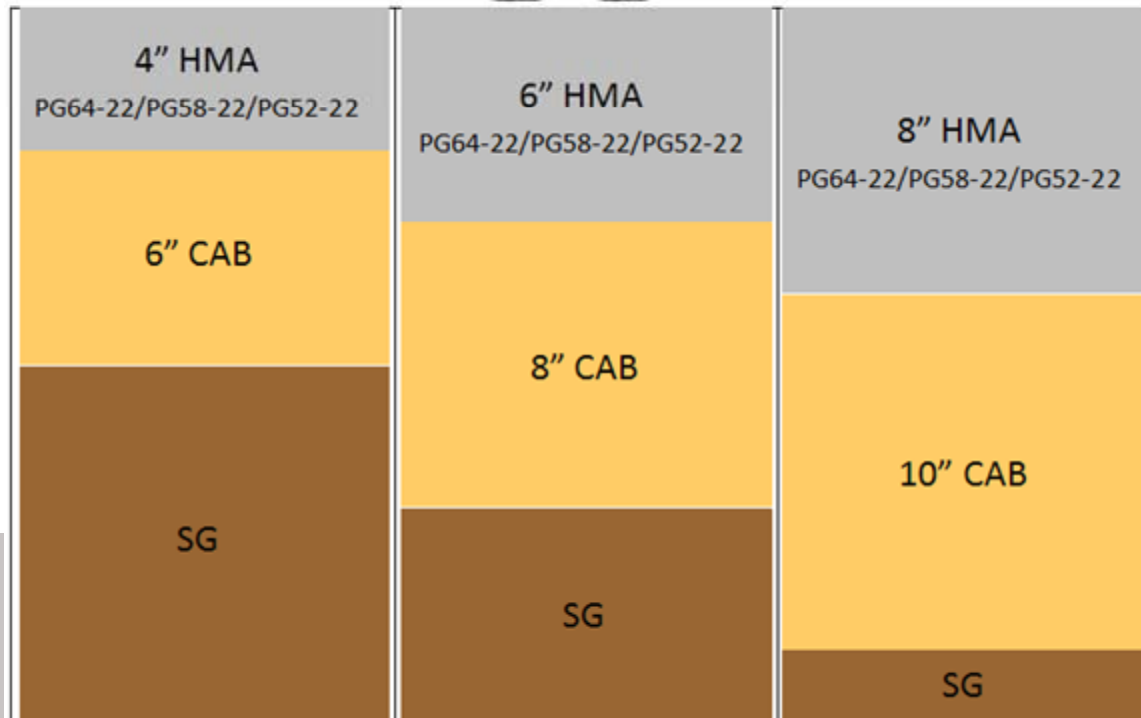
# Database of pavement stresses time-histories



- 60 mph without braking
- 40 mph without braking
- 20 mph without braking
- 2 mph with braking
- 10 mph with braking
- 20 mph with braking



**HMA layer temp:**  
 104 °F, 122 °F,  
 140 °F, and 158 °F



# 3D-Move Model

The image shows a screenshot of the 3D-Move Model software interface. A central blue starburst contains the text "3D-Move Model". Three callout boxes point to specific features: "Complex surface loadings in all three directions.", "Moving loads of any shape (braking forces)", and "Visco-elastic properties".

**Complex surface loadings in all three directions.**

**Moving loads of any shape (braking forces)**

**Visco-elastic properties**

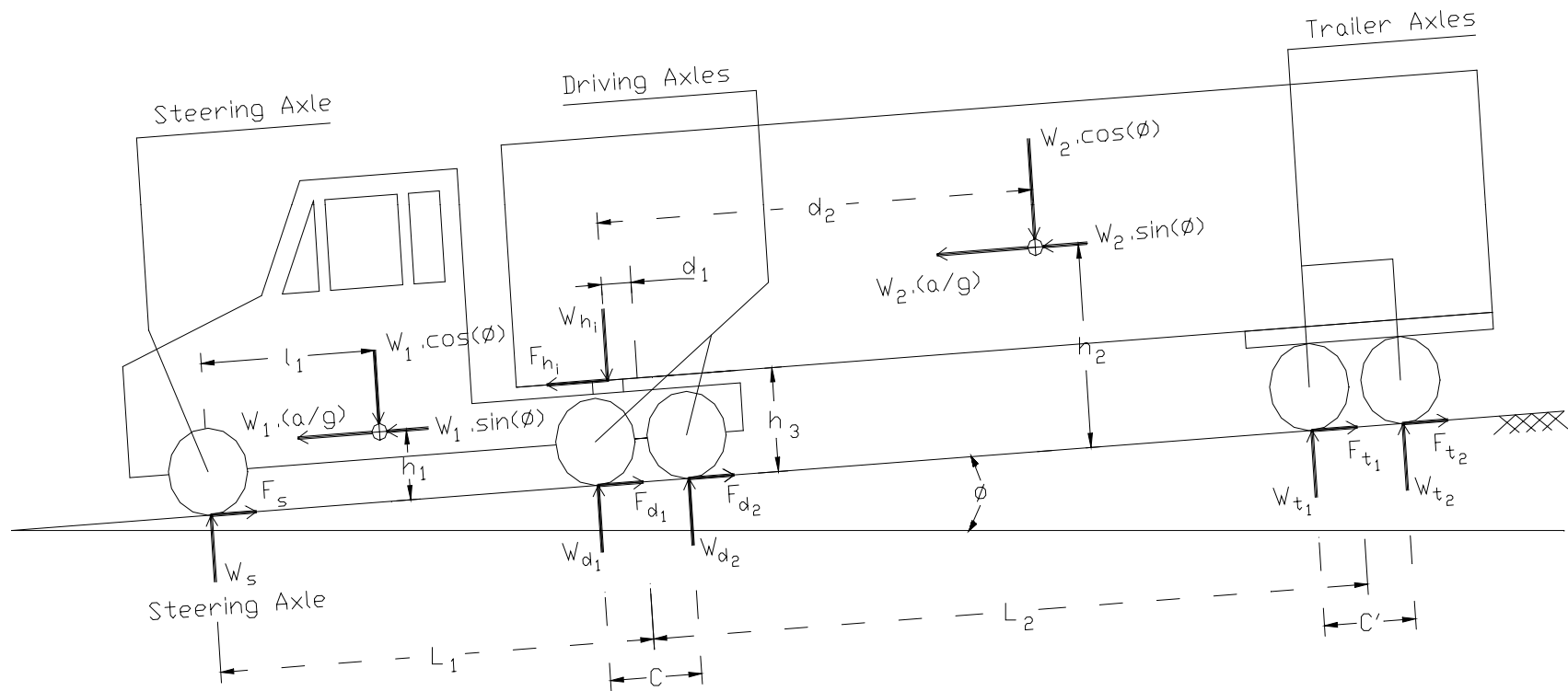
**3D-Move Model**

The software interface includes a menu bar (File, Edit, Tools, Help, UnitConverter), a project tree on the left, and a main workspace. A diagram at the bottom left shows two tires on a road surface with red arrows indicating load distribution. A "Project Information" dialog box is open on the right, showing a table of parameters and values.

Parameter	Value
4-22	
/Units	
ysis - (2mph)	
oad Cases	
(in)	

# Semi-trailer Truck

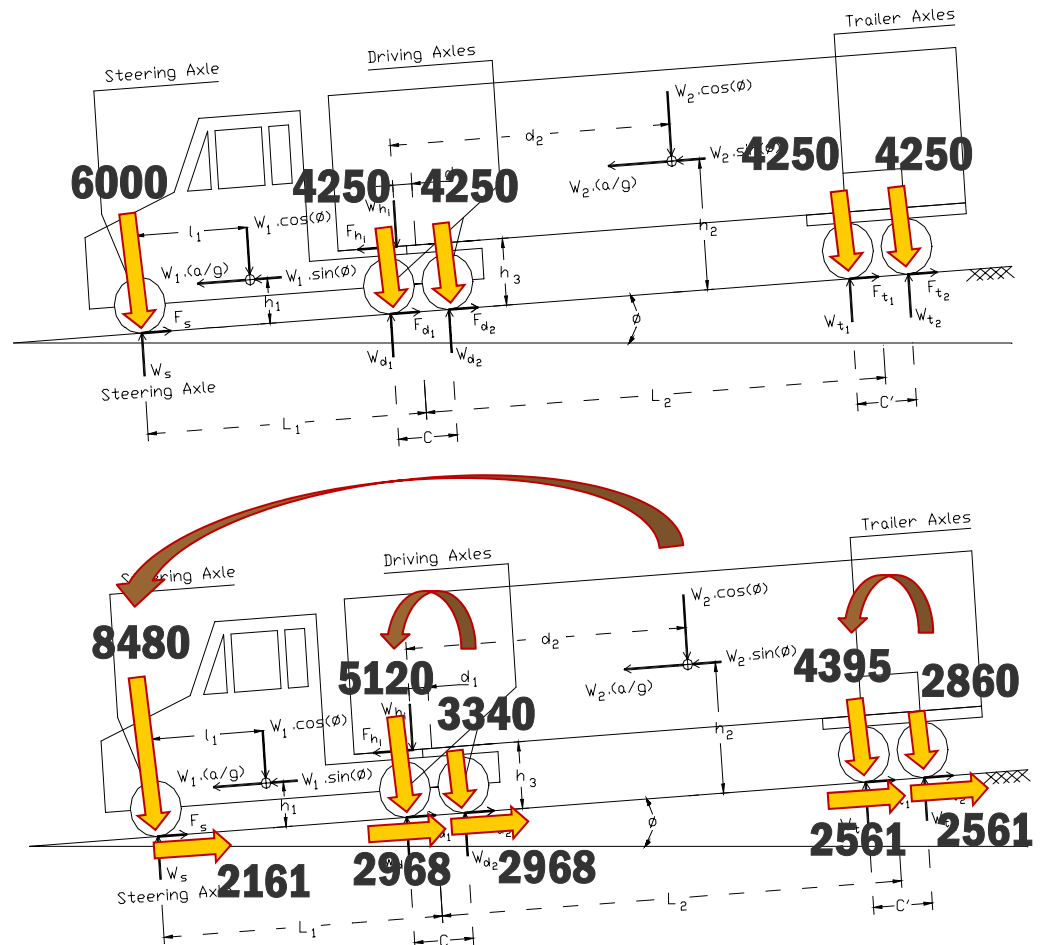
dynamic load transfer → vertical loads on tires additive (+ or -) to static load



**Braking = f(deceleration “a”, braking forces)**

# Semi-trailor Truck

- **Load Distribution During Braking: 14 Unknowns**
  - **11 equilibrium equations**
  - **3 characteristic equations:**
    - **Application (treadle output) vs. actuation (brake chamber) pressure/axle**
    - **Brake force vs. actuation pressure on each axle.**
    - **Dynamic load transfer coefficient.**

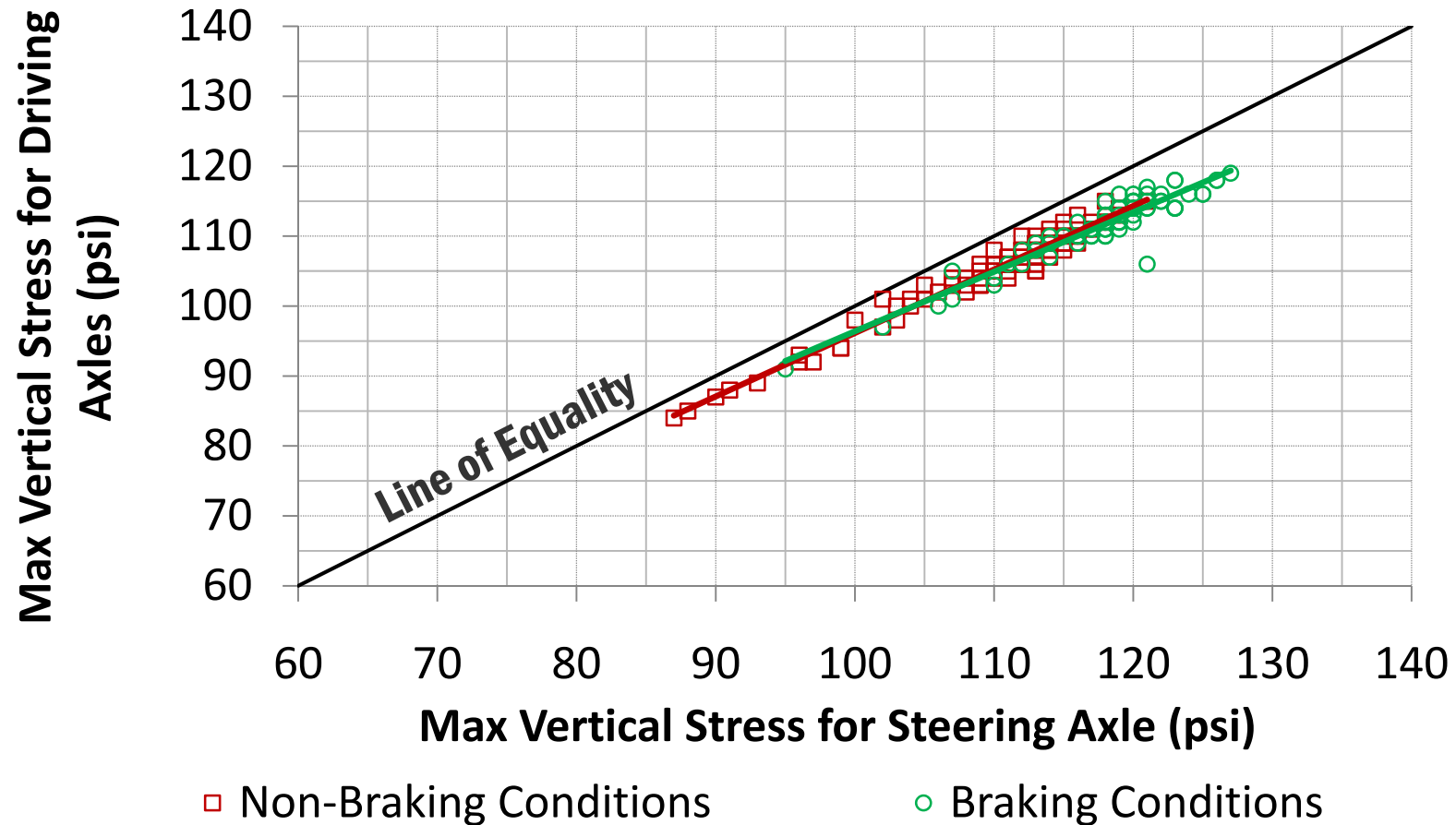


# Equivalent deviator and confining stresses time-histories

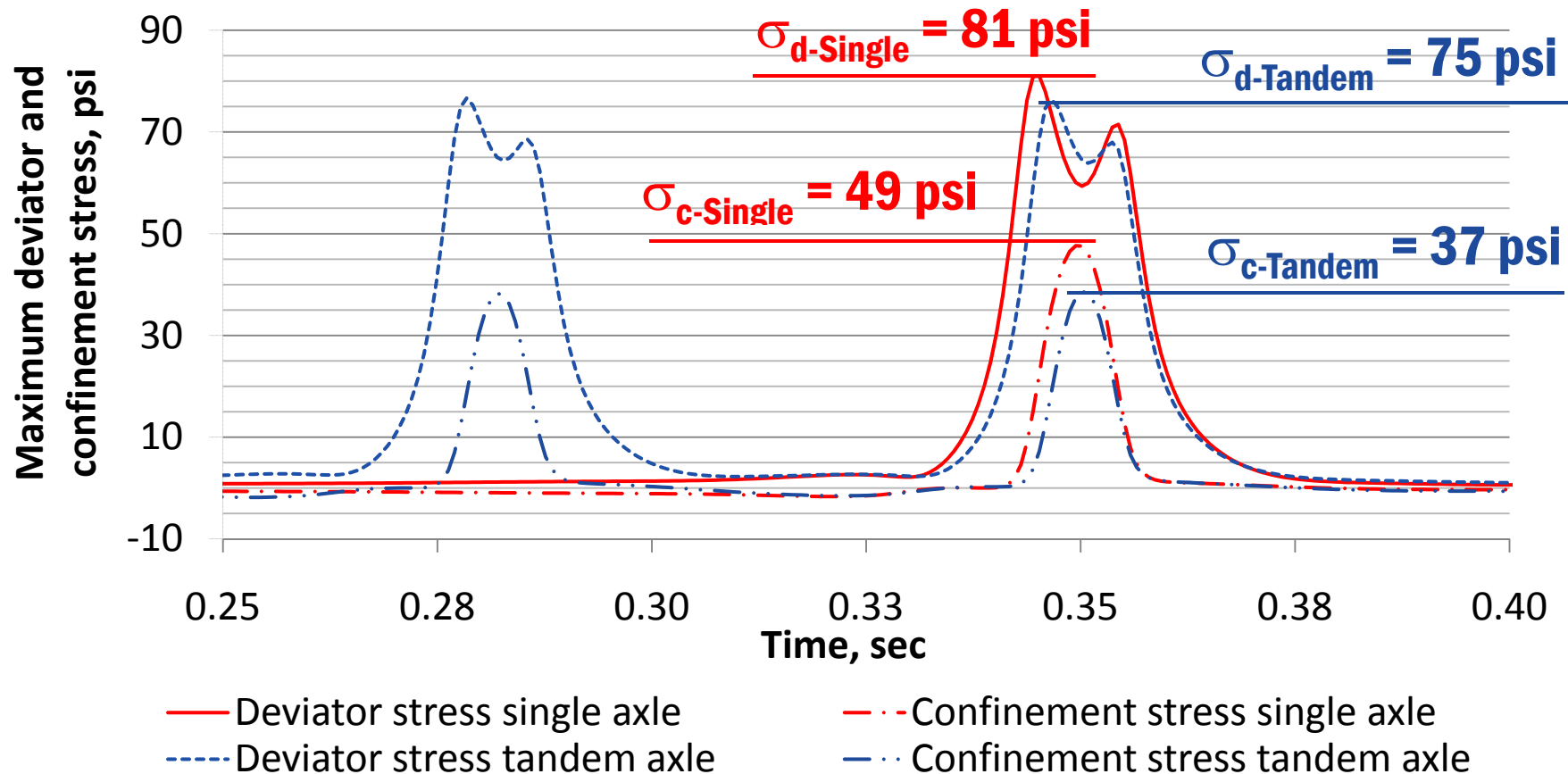
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- $\sigma_d$  &  $\sigma_c$  were analyzed under **Single** and **Tandem** axles for every:
  - pavement structure
  - mixture type
  - pavement temperature
  - braking and non-braking conditions.

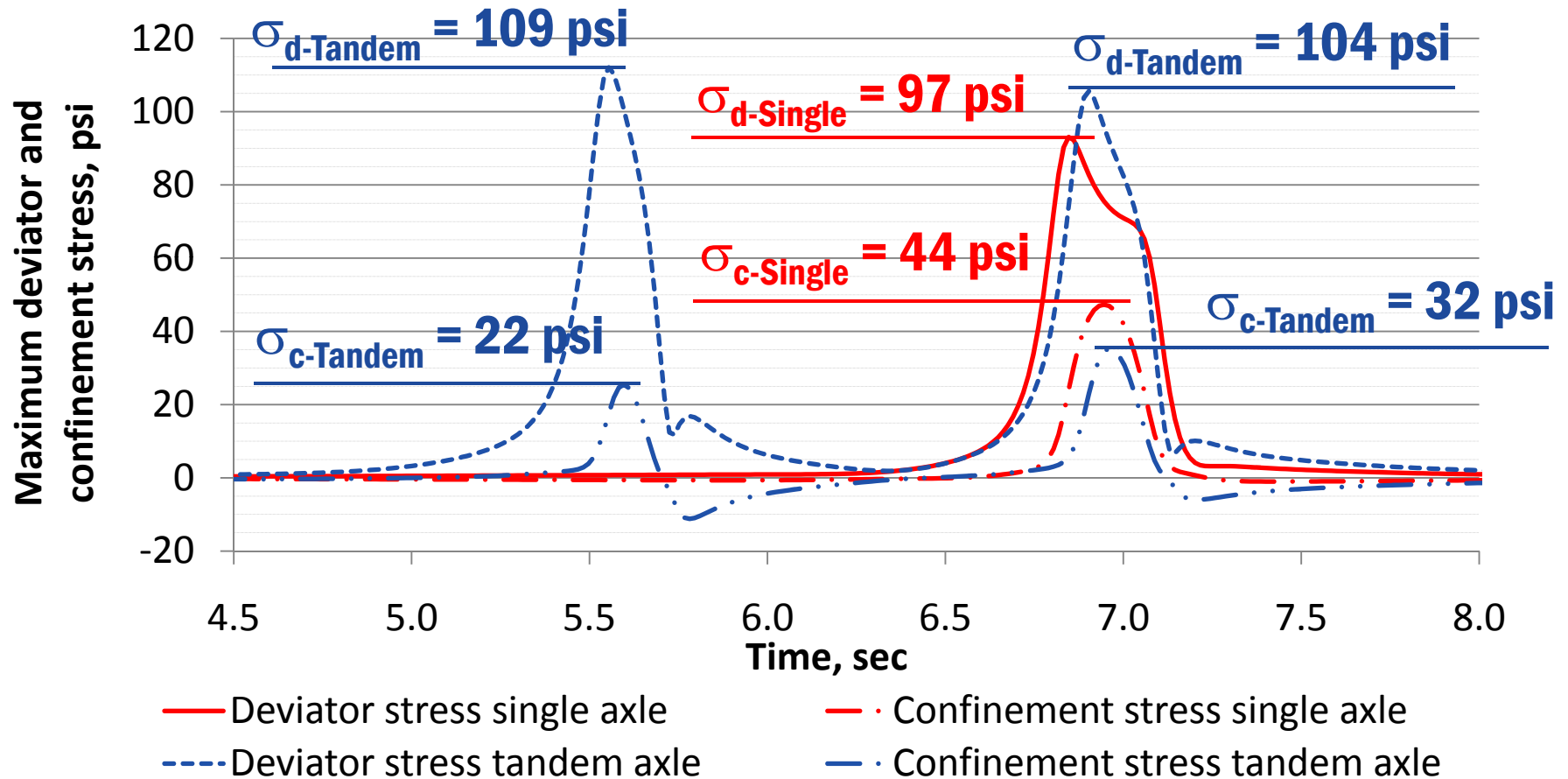
# Equivalent deviator and confining stresses time-histories Single vs. Tandem Axles



# Equivalent deviator and confining stresses time-histories Single vs. Tandem Axles (Non-braking)



# Equivalent deviator and confining stresses time-histories Single vs. Tandem Axles (Braking)



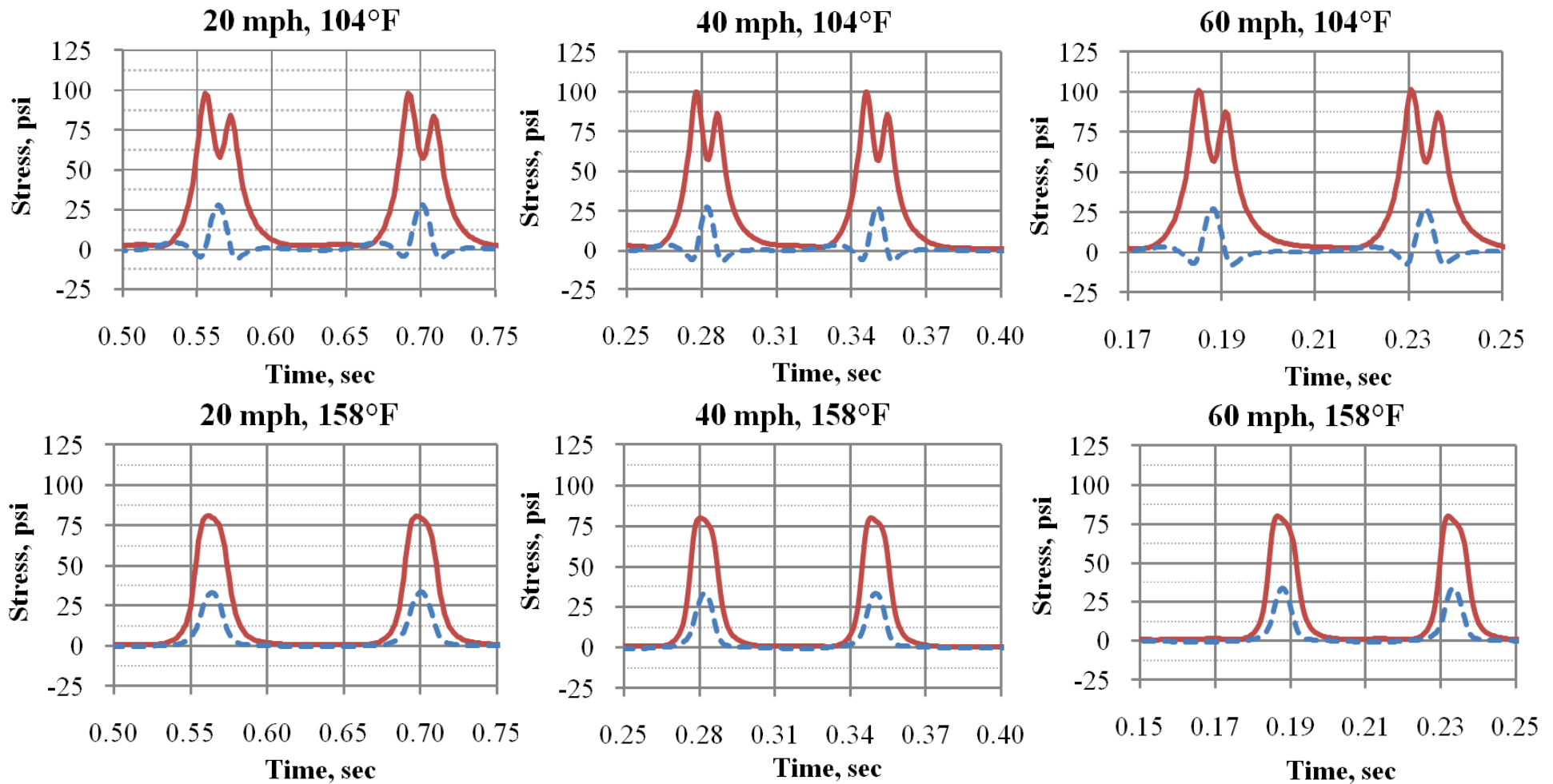


# Equivalent deviator and confining stresses time-histories

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- **Tandem axle generates a more critical stress condition than the steering axle when the 3D state of stresses is analyzed.**
- **Stresses evaluated under tandem axles at 2-inch below pavement surface.**

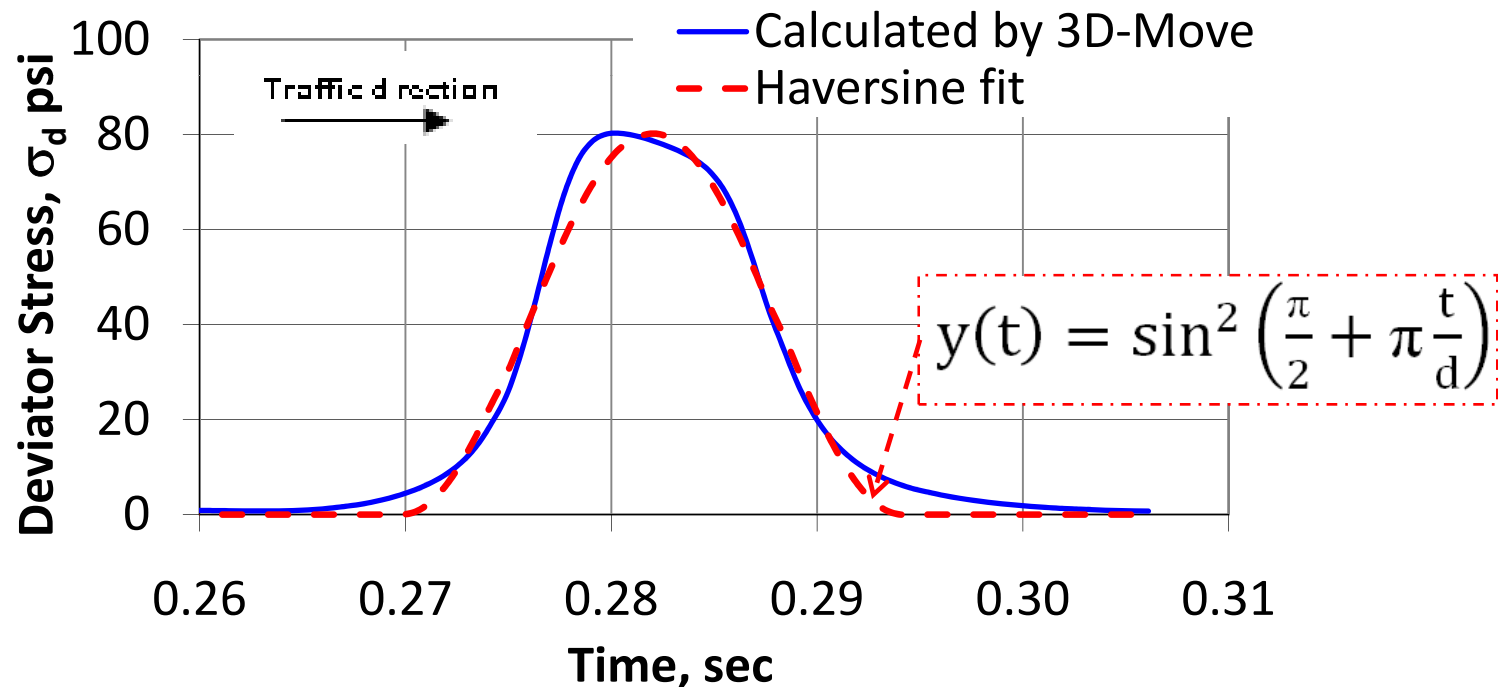
# Equivalent deviator and confining stresses time-histories



— Deviator Stress  
- - - Confining Stress

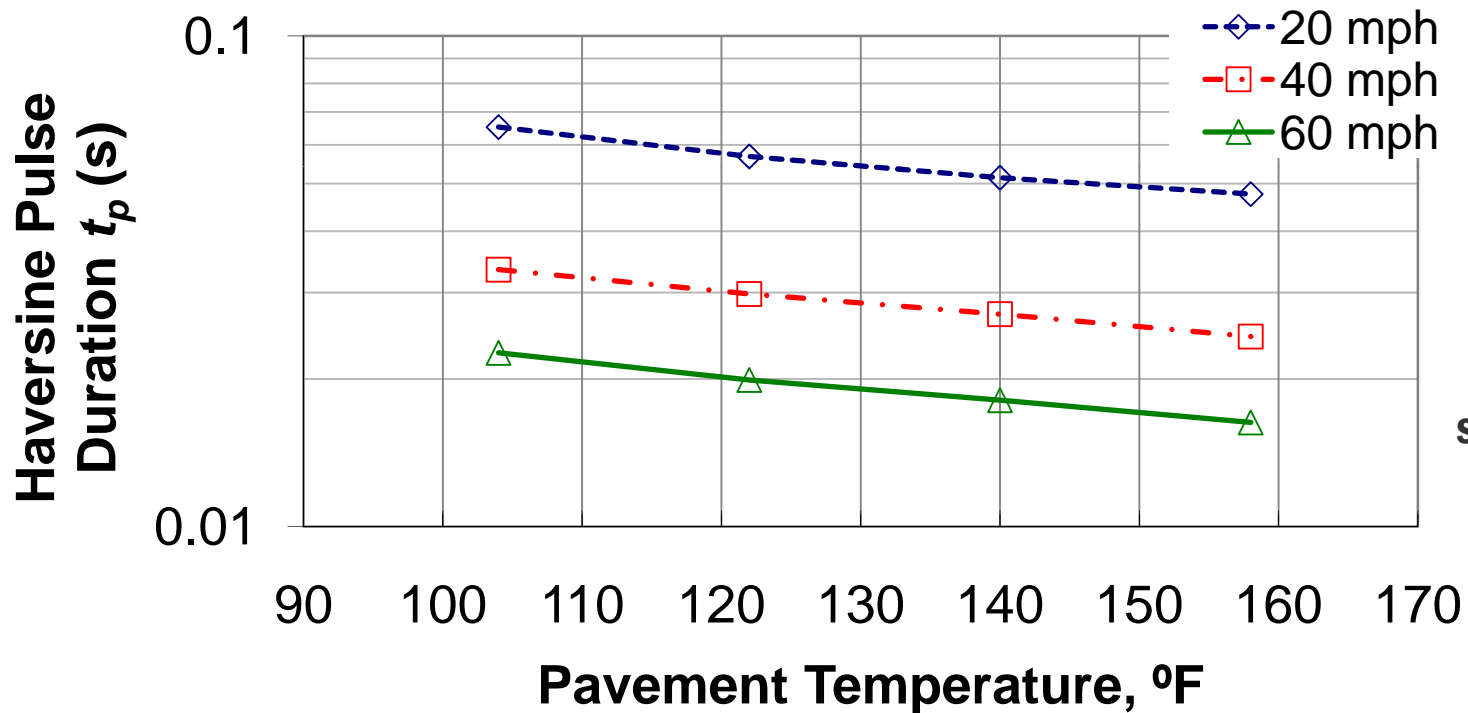
# Equivalent deviator stress pulse duration

- Loading pulse characterized using  $\sigma_d$  at 2 inches.
- Best-fitting haversine wave shape.



# Equivalent deviator stress pulse duration *under tandem axle, 2 inches below pavement surface*

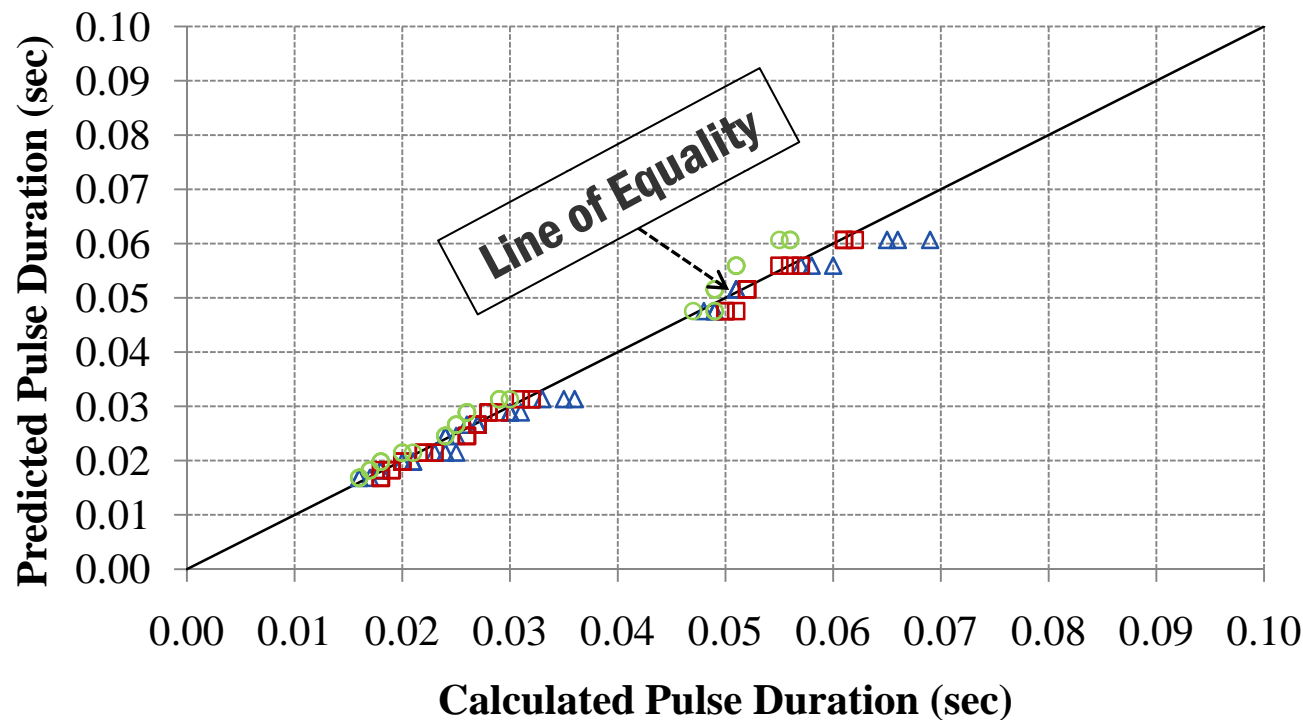
## PG64-22 Mix Non-braking



Pavement  
structure: 4" HMA  
over 6" base

## Equivalent $t_p$ at 2" below pavement surface Non-braking Conditions (20-60 mph, 104-158°F)

$$\log(t_p) = -0.00353(T) - 0.0236(S) + 0.00015(S)^2 - 0.6654$$

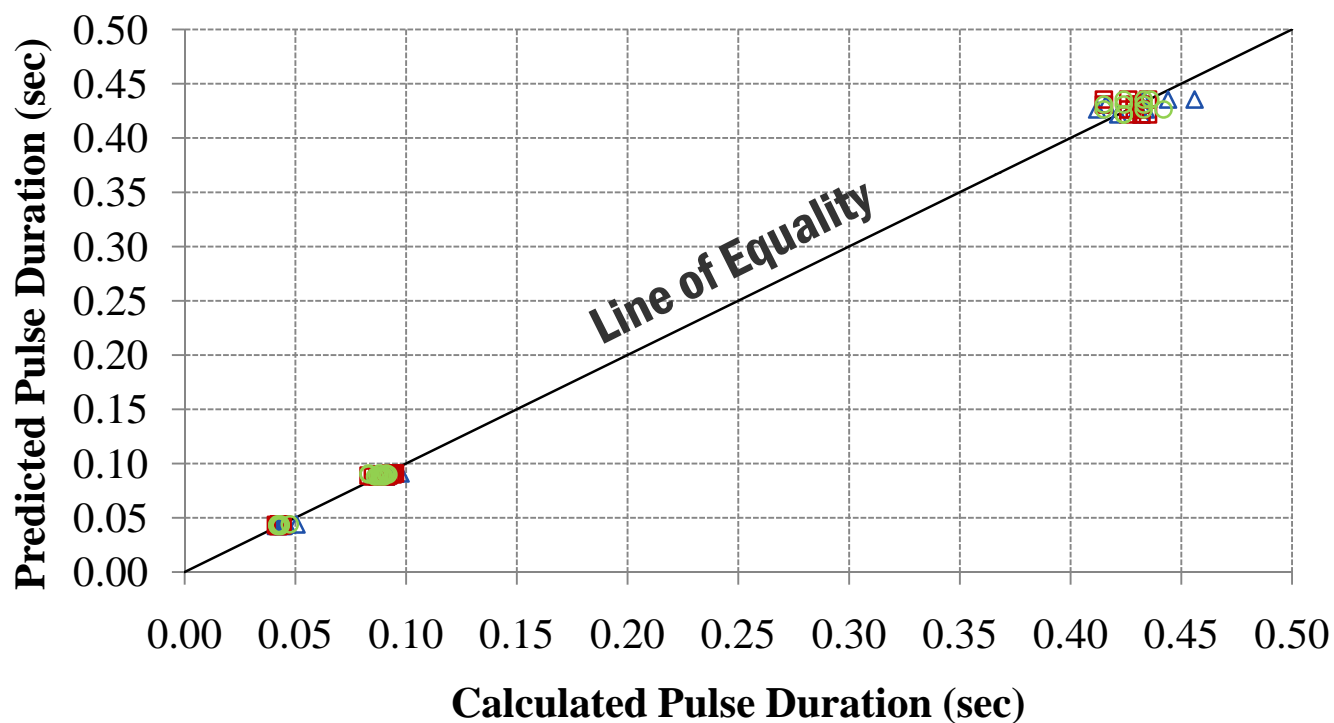


- $T$  = asphalt layer temperature, °C
- $S$  = vehicle travelling speed, mph.

△ PG64-22 (Non-braking)    □ PG58-22 (Non-braking)    ○ PG52-22 (Non-braking)

## Equivalent $t_p$ at 2" below pavement surface Braking Conditions (2-20 mph, 104-158°F)

$$\log(t_p) = -0.000387(T) - 0.05531(S) - 0.23603$$



- $T$  = asphalt layer temperature, °C
- $S$  = vehicle travelling speed, mph.

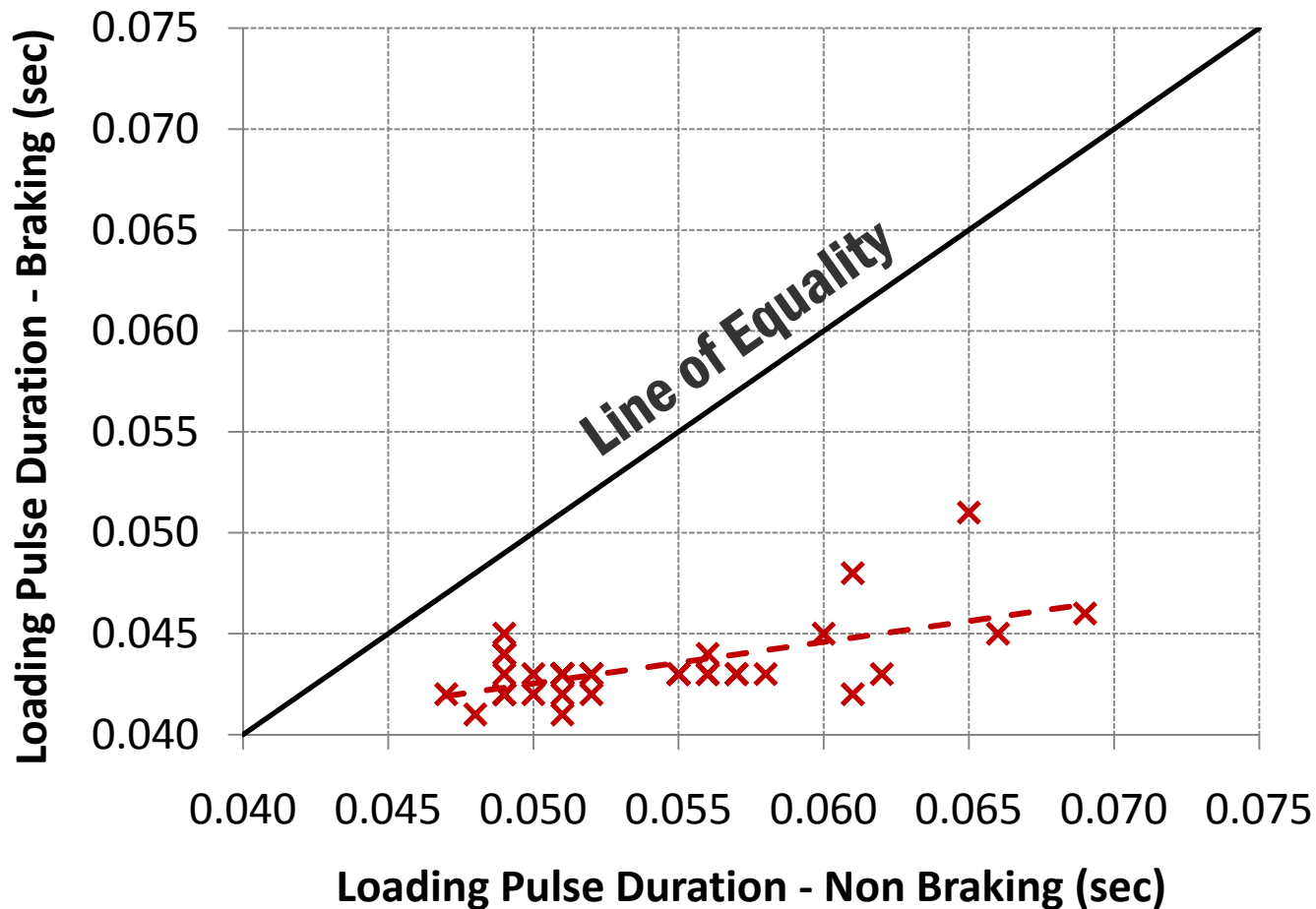
△ PG64-22 (Braking)    □ PG58-22 (Braking)    ○ PG52-22 (Braking)

# Equivalent Deviator Stress Pulse Duration ( $t_p$ ) at 2" below pavement surface

	Non-Braking	Braking
Speed	20-60 mph	2-20 mph
Equivalent Deviator stress pulse ( $t_p$ )	0.016-0.069 sec	0.041-0.456 sec

**< 0.1 sec typically applied to FN test  
(*except for braking at 2 mph*)**

# Equivalent deviator stress pulse duration Braking vs. Non-braking at 20 mph

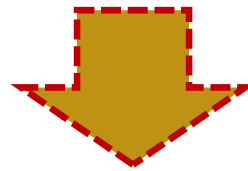


12% to 29%  
reduction in  
pulse time

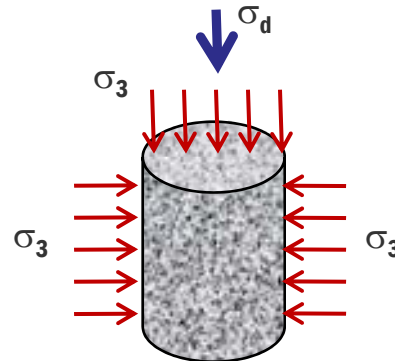


# Equivalent Deviator Stress Pulse Duration ( $t_p$ ) at 2" below pavement surface

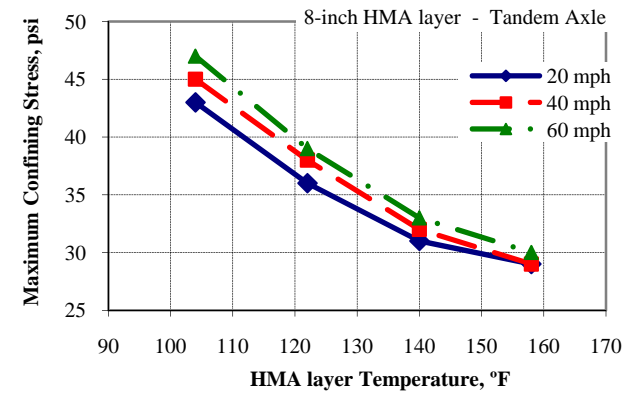
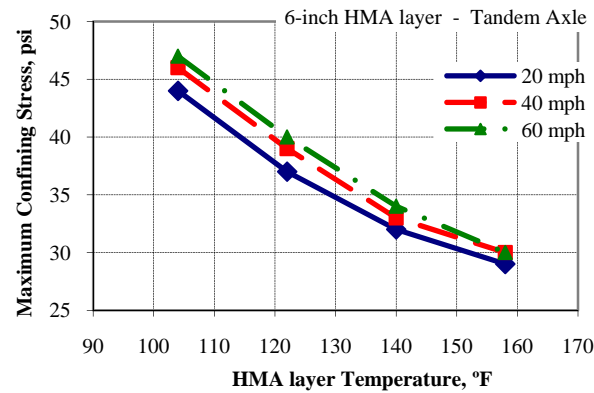
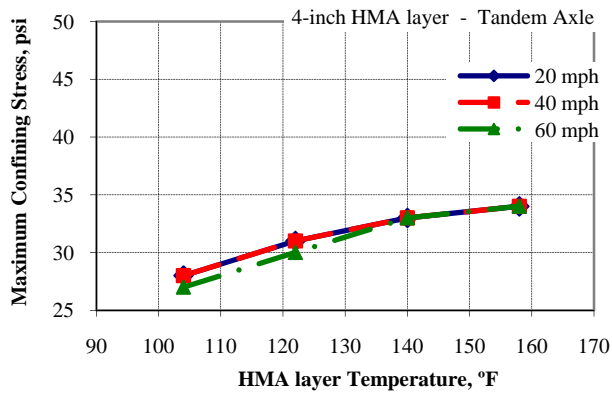
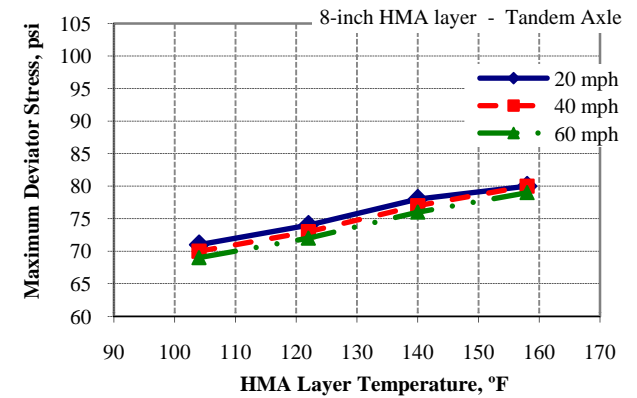
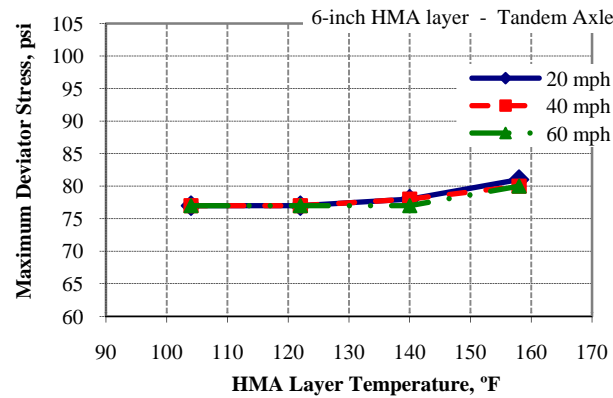
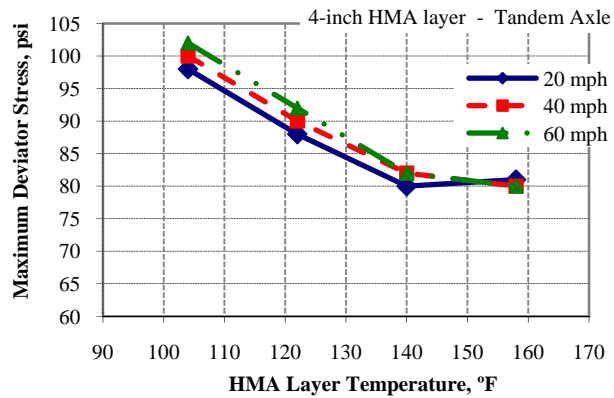
Non-braking condition seems to result in a more critical condition than braking condition.



*Evaluate the magnitudes of  $\sigma_d$  and  $\sigma_c$  under braking and non-braking conditions*

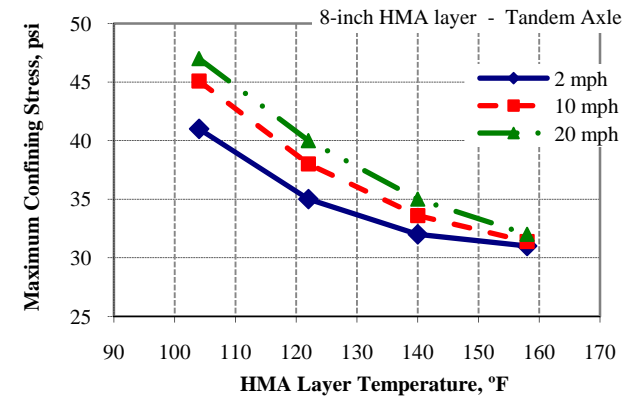
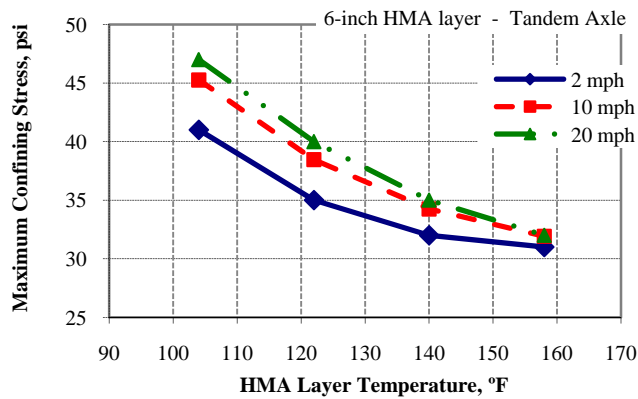
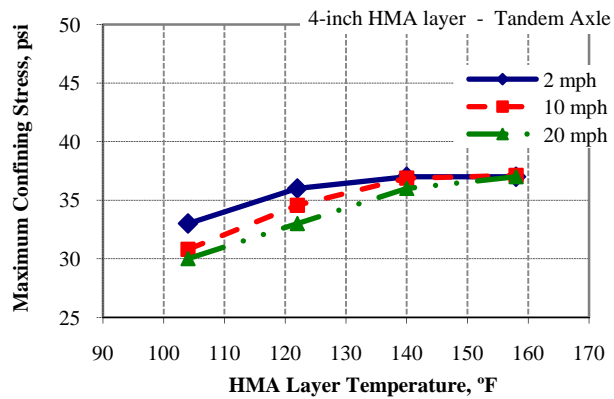
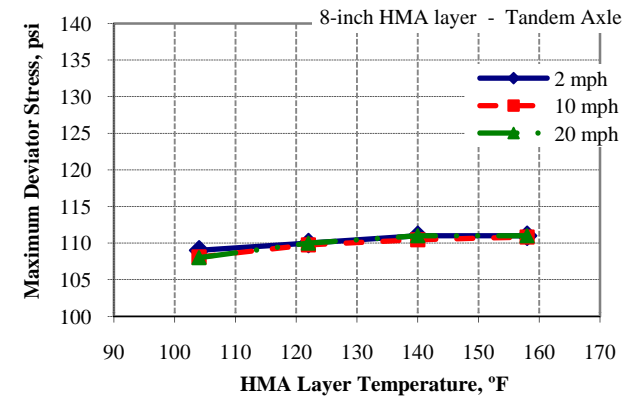
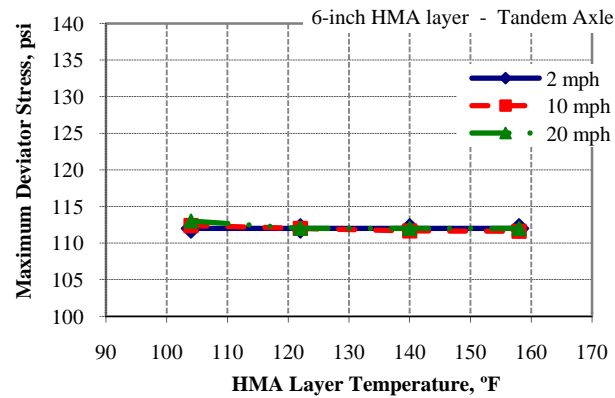
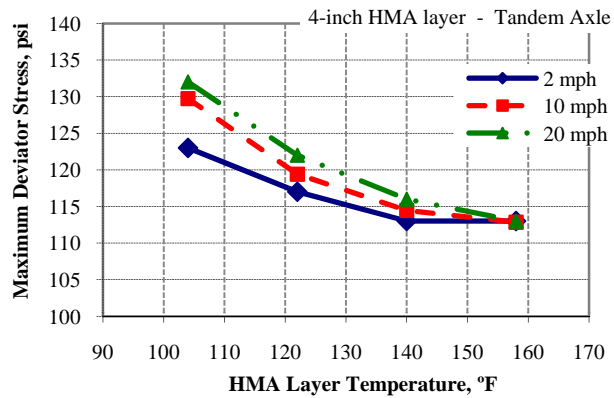


# Maximum equivalent $\sigma_d$ and $\sigma_c$ stresses



PG64-22 Mix for non-braking conditions

# Maximum equivalent $\sigma_d$ and $\sigma_c$ stresses



PG64-22 Mix for braking conditions

# Maximum equivalent $\sigma_d$ and $\sigma_c$ stresses

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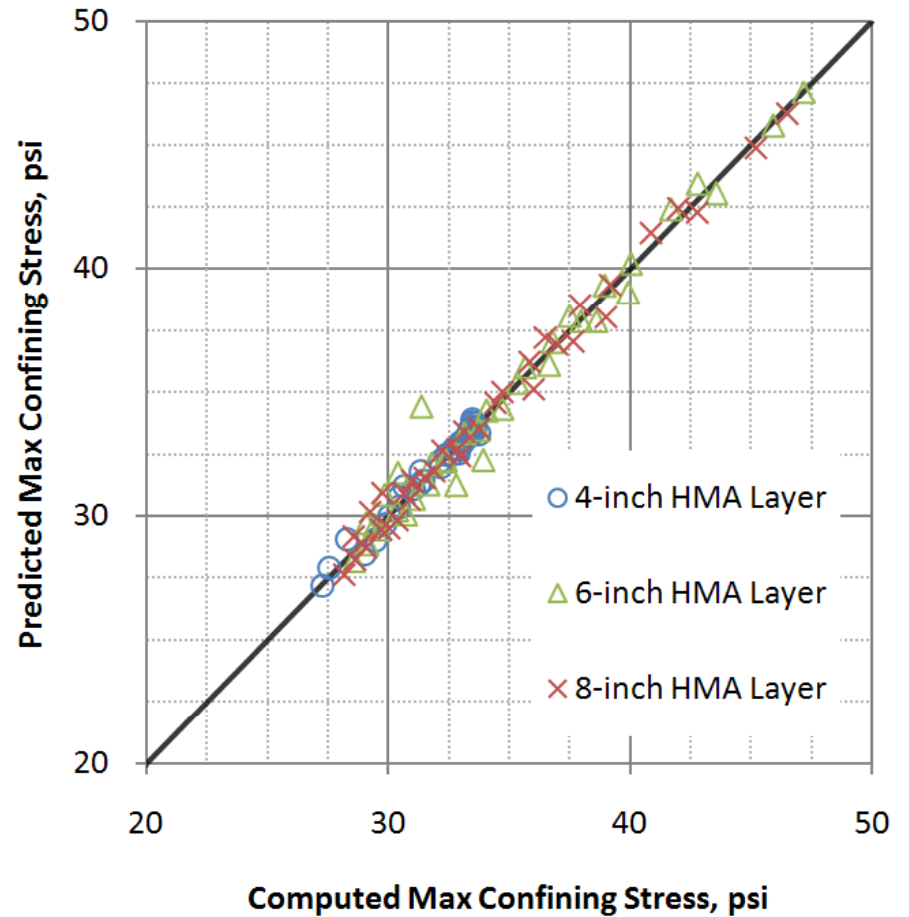
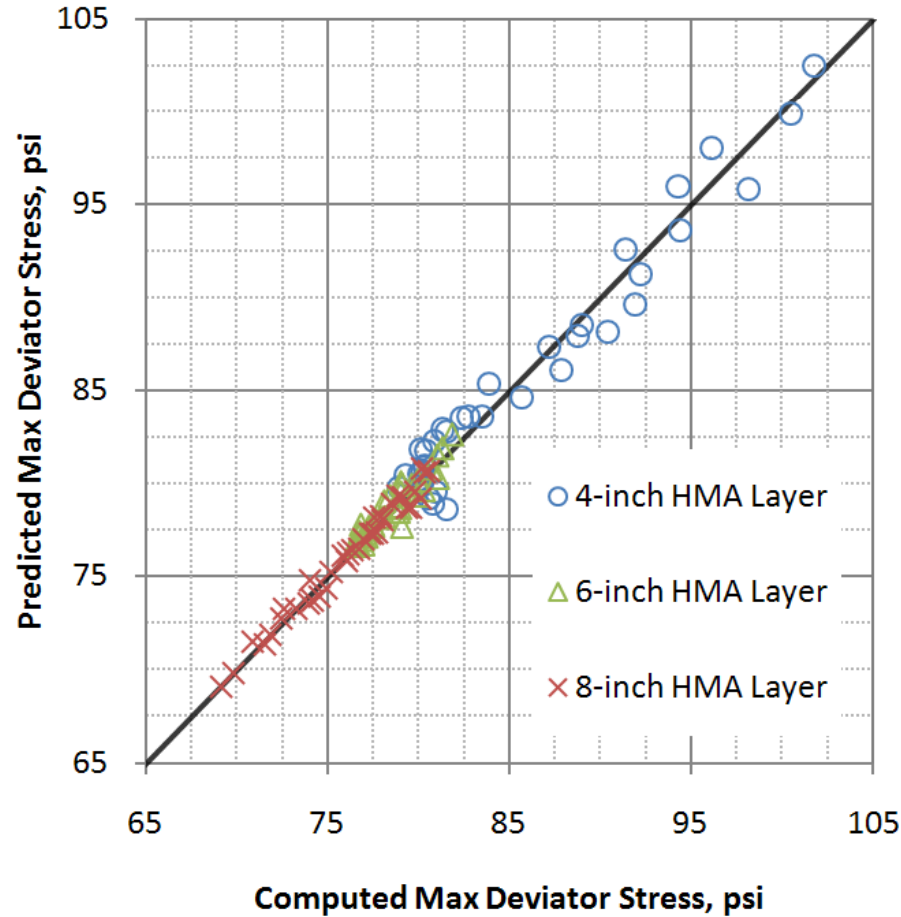
- Predictive Equations for:
  - Equivalent max deviator stress,  $\sigma_d$
  - Equivalent max confining stress,  $\sigma_c = \sigma_3$

*at 2 inches below pavement surface*  
*Braking and Non-Braking Conditions*

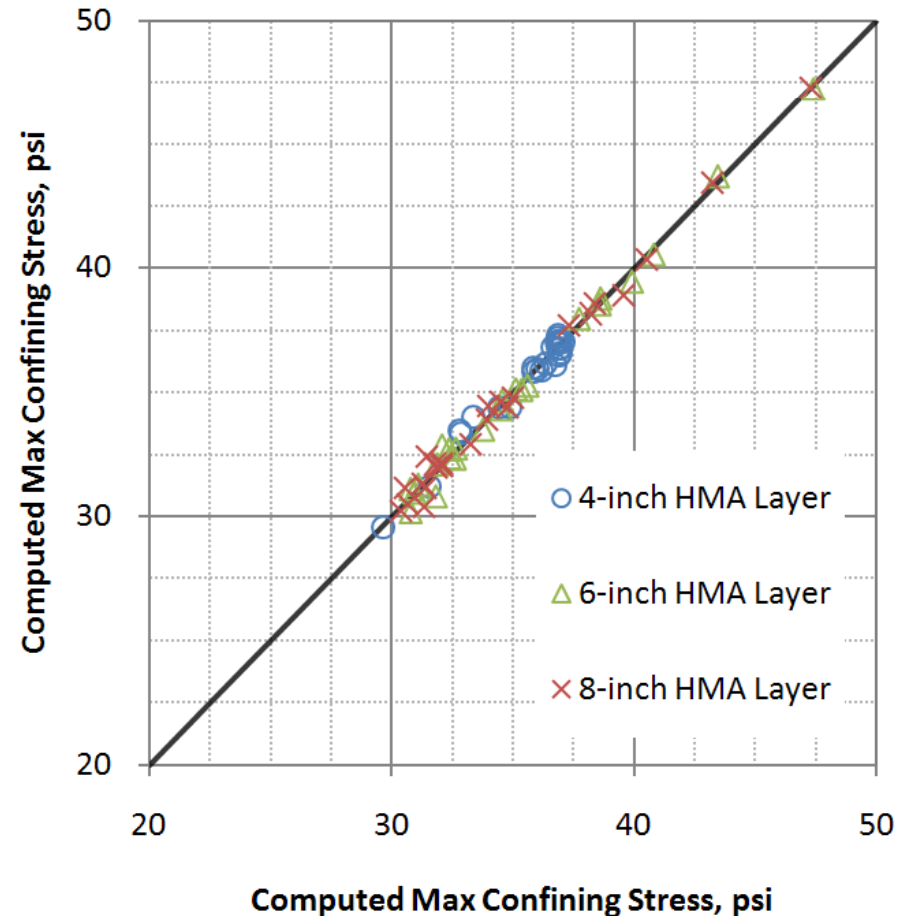
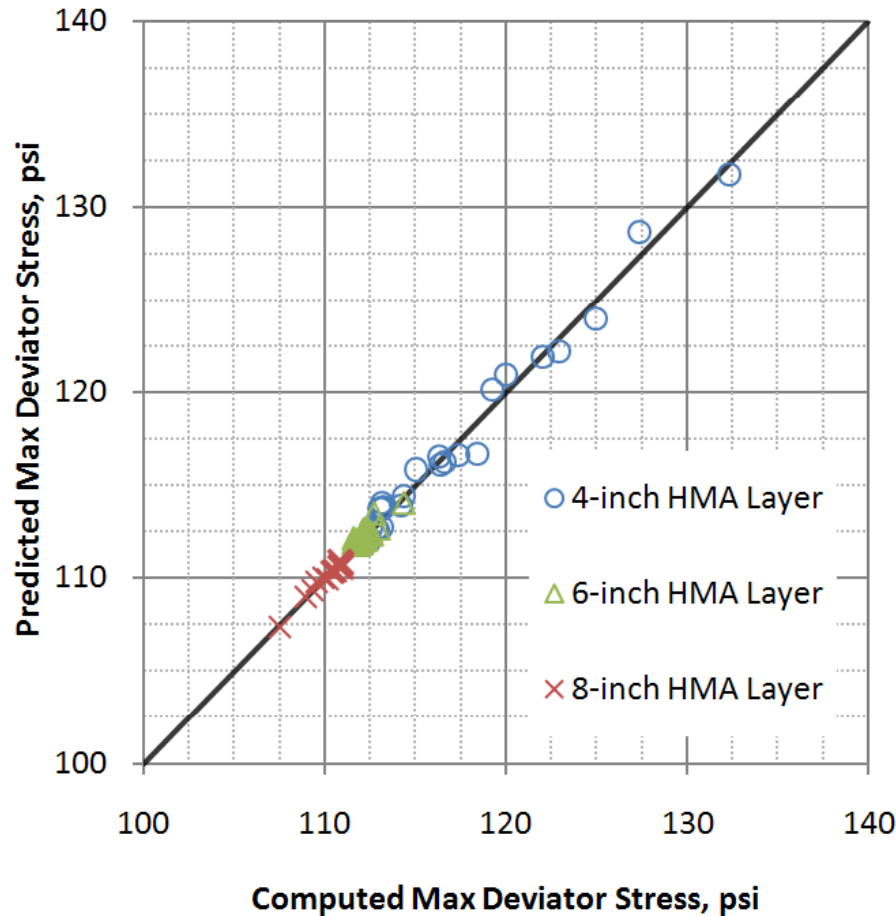


**Function of *AC layer thickness,  $T$ ,  $E^*$ ,  $S$ , interaction terms***

# Equivalent Deviator & Confining Stresses at 2" Non-Braking Conditions



# Equivalent Deviator & Confining Stresses at 2" Braking Conditions



# Equivalent Deviator & Confining Stresses at 2" Below Pavement Surface

## Non-braking conditions:

- $\sigma_d$  ranged from 69 to 102 psi
- $\sigma_c$  ranged from 27 to 47 psi

slight increase  
(5%) in  $\sigma_c$

## Braking conditions:

- $\sigma_d$  ranged from 108 to 132 psi
- $\sigma_c$  ranged from 30 to 47 psi

40% increase  
in  $\sigma_d$

# Summary and conclusions

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- **Equivalent deviator stress pulse duration ( $t_p$ ) at 2” below the pavement is function of**
  - **vehicle speed, and**
  - **pavement temperature.**
- **Neither pavement thickness nor mixture properties significantly impacted  $t_p$  at 2” below pavement surface.**



# Summary and conclusions

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- **Standard pulse time loading of 0.1 sec does not simulate actual traffic-induced deviator stress pulse duration.**
- **Braking conditions, though it generates interface shear stresses, leads to lower deviator pulse duration & higher amplitude.**

# Summary and conclusions

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- **Amplitude of the equivalent triaxial deviator and confining stresses are highly affected by:**
  - **Mixture's stiffness**
  - **Pavement effective temperature**
  - **Vehicle speed.**

# Thank you for your attention!!!

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- **Acknowledgments**

- This work is part of the overall effort in the Asphalt Research Consortium (ARC) work element E2c: “Critically Designed HMA Mixtures.” ([www.arc.unr.edu](http://www.arc.unr.edu))
- Authors gratefully acknowledge the FHWA support.